

WINTER TEMPERATURE STRUCTURE OF LAKE MICHIGAN

Vincent E. Noble

Karen J. Ewing

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## INTRODUCTION

This is the final report on Atmospheric Sciences Section, National Science Foundation Grant GA-524, a two-year research project designed to investigate the winter thermal budget of the Great Lakes (principally Lake Michigan), as a necessary sequel to a previous project supported by the Atmospheric Sciences Section of the National Science Foundation under NSF Grant GP-2411, titled "Growth of Ice on Lake Michigan." The final report of the previous project was published in 1966 as Special Report No. 26 of the Great Lakes Research Division of the University of Michigan (Heap and Noble 1966). The first annual report of this project was published as Special Report No. 32 of the Great Lakes Research Division (Noble and Ewing 1967). A related study of the summer temperature structure of Lake Michigan for 1963-66 was carried out under the cognizance of the current project, and was reported in Special Report No. 30 of the Great Lakes Research Division (Noble 1967).

Inasmuch as this is the final report for the research project, the previous results will be summarized, as necessary, for completeness. New data and analyses will be presented in detail. Readers may obtain copies of previous reports from the Great Lakes Research Division for full data reports published earlier.

Two graduate students have participated heavily in this project and have made significant contributions to the results of the program: Joseph C. Huang, who has done much of the computer programming and who is doing a related dissertation problem, and Karen J. Ewing, co-author of this report. Of the three undergraduate students working on the project, April Michaelis has made a most valuable contribution and has co-authored a related data report, Special Report No. 39 of the Great Lakes Research Division (Noble and Michaelis 1968).

## ICE PREDICTION INDICES

The research program supported by this grant was designed to verify potential ice prediction techniques indicated by a previous study reported by Heap and Noble (1966).

Within constraints to be described in following sections of this report, and within verification conditions imposed by the somewhat limited ice cover observations for Lake Michigan, an operational ice prediction technique is promulgated for initial implementation by the U.S. Coast Guard, U.S. Weather Bureau, and the Lake Carriers Association. The operational method is initially designed for Lake Michigan, with the understanding that the basic methods may be subsequently applied to all of the Great Lakes as substantiating data are developed. It is suggested that the technique be extended to the remainder of the Great Lakes with the cognizance and cooperation of the Canadian Department of Transport.

### *Ice Potential Index*

As indicated in the previous study, and as verified for a five-year period (Noble and Ewing 1967), the early-winter temperature structure of Lake Michigan may be used as an indicator of the ice-forming potential of Lake Michigan.

If the temperature of the mid-lake water mass (the deep portions of the southern basin of the lake) is of the order of 9°C for the first week of December, there is sufficient heat storage in the lake to reduce ice formation to a nearly insignificant amount (e.g. the winter season of 1963-64). If the temperature of the mid-lake water mass is of the order of 6°C for the first week of December, ice formation may approach 100% coverage of the lake basin (e.g. the winter season of 1962-63). These criteria were established from weekly averages calculated from U.S. Public Health Service Federal Water Pollution Control Administration buoy stations in Lake Michigan.

BT data from the USCGC WOODBINE, taken during her late November-early December run to recover aids to navigation in the southern basin of Lake Michigan, have served as a useful approximation to average thermograph data for an Ice Potential Index. Further, since the water column of the lake is nearly isothermal at this time of year, it has been demonstrated that accurately calibrated surface temperature measurements taken from the WOODBINE may be used as the Ice Prediction Index. (An accurate, calibrated, thermistor bridge was installed in the main sea chest of the WOODBINE in the fall of 1967.) Table 1 summarizes the Ice Potential Index data for the winter seasons 1962-63 through 1967-68.

The following technique is suggested for the determination of an annual Ice Prediction Index for Lake Michigan:

A calibration check should be run on the WOODBINE'S thermistor bridge during early November. During the fall cruise to recover aids to navigation (typically Grand Haven - Milwaukee - Chicago - Grand Haven during the last week of November and the first week of December), the WOODBINE should read

Table 1. Ice Potential Index data for winter seasons 1962-63 through 1967-68.

1962-63	Average water temperature 5.9°C, 2 December-9 December 1962, buoy station 18 (43°08'N, 57°24.5'W). Ice potential: Heavy. Ice cover: Record ice formation.
1963-64	Average water temperature 8.8°C, 2 December-9 December 1963, buoy station 18 (43°08'N, 57°24.5'W). Ice potential: Light. Ice cover: Very light ice formation.
1964-65	No water temperature measurements.
1965-66	WOODBINE BT's water temperature 7.3°C to 9.4°C, Southern Basin Lake Michigan, 3 December-9 December 1965. Ice potential: Light. Ice cover: Very light ice formation.
1966-67	WOODBINE BT's water temperature 4.2°C to 8.2°C, 3 December-9 December 1966, Southern Basin Lake Michigan. Ice potential: Moderate. Ice cover: Moderate to light.
1967-68	WOODBINE BT's and thermistor bridge 3.5°C to 5.3°C, 13 December-18 December 1967, Southern Basin Lake Michigan. Ice potential: Heavy. Ice cover: Early ice melted mid-winter. Later ice held to late in season.

surface water temperatures from her thermistor bridge (to the nearest 0.1°C) at each point of departure upon entering and leaving harbor entrances, and at each hour while away from the dock. Each day (say at 1000 hours, depending upon traffic) the WOODBINE should transmit a message to 9th District Coast Guard Headquarters giving the surface water temperature readings for the preceding 24 hours. The message would be coded in the following format:

LLLL 1111 ttt, LLLL 1111 ttt, ...

where LLLL is the latitude in whole degrees, minutes, and tenths of minutes (omitting the ten-degree digit 4)

where 1111 is the longitude in whole degrees, minutes and tenths of minutes (omitting the ten-degree digit 8)

where ttt is the water surface temperature to 0.1°C.

Upon receipt of the coded message at Coast Guard headquarters in Cleveland, the WOODBINE temperatures would be given a subjective analysis to derive the Ice Prediction Index. Subjective analysis is required to interpret the temperatures obtained around the southern basin of Lake Michigan in terms of a temperature representative of the deep-water mass of the lake. In other words, ship injection temperatures are used to approximate the weekly average, deep-water thermograph data obtained in 1962-63 and 1963-64. Equivalent deep-water temperatures (representative of the southern basin of the lake), between 6°C and 9°C for the first week in December, indicate a potential for the formation of an ice cover ranging from extremely heavy to very light, respectively.

It is strongly suggested that all of the Coast Guard cutters on the Great Lakes be provided with precision water intake temperature indicators similar to that installed on the WOODBINE, and that similar statistics be developed for Ice Potential Indices for all of the Great Lakes.

#### *Freeze-up Date and Rate of Ice Formation*

Verified statistics have not been developed, but a method similar to that of Richards (1964) has been indicated for the short-range (one week) prediction of the freeze-up date and the rate of ice formation of Lake Michigan. This technique is based on the analysis of daily air temperature data from Milwaukee. As will be developed in a following section of this report, the method is to compute the mean of the high and low temperature for each day, convert this mean to temperature expressed in degrees Celsius, and maintain a cumulative plot of the sum of the daily mean temperatures from 1 October of each year. Since the freezing point is 0°C, the cumulative plot represents degree-days of freezing (or thawing) exposure. The cumulative plots (Noble and Ewing 1967; Heap and Noble 1966) show a positive increase from 1 October until approximately 25 November, when a maximum is reached. The curve then goes negative from the last week in November, indicating the onset of freezing weather. The date of the maximum of the curve is a precursor of the freeze-up date, and the rate of decrease of the cumulative curve indicates the rate of ice formation. The curve begins to decrease as negative degree-days (freezing exposure) are algebraically added to the cumulative curve.

Inadequate ice observations over a sufficient period of record for Lake Michigan have prevented the establishment of empirical criteria for the definition of freeze-up dates or of the rate of ice formation. These data are currently being developed through systematic ice observations being carried out by the U.S. Lake Survey.

The Ice Prediction Index provides an estimate of the amount of ice to be expected in any given season. The cumulative Celsius degree-day plots provide an indication of the freeze-up date, and the rate of formation of ice to the predicted maximum.

The long-range warming or cooling trend of Lake Michigan may be estimated for four-year periods by the method of Ayers (1965).

## A PRELIMINARY STUDY OF THE LAKE MICHIGAN HEAT BUDGET

Ayers (1965) suggested that annual averages of air temperatures, cloudy days, and storm passages over the Lake Michigan basin can be combined as moving 5-year means to predict warming and cooling trends of the water temperatures measured at the Chicago water intakes. These climatological calculations have been carried out from data available for the last century, and indicate the observed water temperature trends approximately five years in advance. Ayers' resultant predictor curve has been extended to 1965, and is reproduced in Figure 1. The predictor curve indicates that the lake should cool and remain at lower temperatures through approximately 1970. Table 1 showed a cooling trend from 1965 through 1967. It is anticipated that the lake will remain at low temperatures for another two years.

In order to study the heat storage in the lake basin, a computer program has been developed to analyze all BT data from the Great Lakes Research Division for monthly average water temperatures for 10-meter layers for each month for each one-degree latitude/longitude square in the Lake Michigan Basin. The data have been published for 1963-1966 by Noble (1967). The BT punch card format used by the Great Lakes Research Division, the analysis program, and the data for 1954, 55, 61, 62, and 1967 (all available data) are presented in Appendix B.

A second program has been developed that analyzes each individual BT cast, determines whether a thermocline exists, or whether the cast is isothermal, and defines the upper and lower limits of the boundary layer and the depth of maximum temperature gradient. The analysis program and the summary data giving the limits of the boundary layer and the depth of maximum gradient by month for each degree of latitude of Lake Michigan for 1954 through 1967 are presented in Appendix C.

Because of the lack of winter water temperature data (except for the 1962-63 and 1963-64 seasons) and because of the lack of complete ice reconnaissance data for the whole Lake Michigan basin, the winter heat transfer from the water mass of Lake Michigan must be estimated from fall lake temperatures, spring lake temperatures, and the sensible heat transfer into the air mass as it crosses the lake under the effect of the prevailing westerly winds. This estimate of heat transfer does not provide adequate data for heat budget calculations, but may be used to estimate trends in the heat storage in the lake. In order to measure the solar radiation available for lake heating during the winter, integrating solar radiometers were developed and tested in the Ann Arbor area during the winter of 1966-67, as described in the previous report. The integrating radiometers were modified slightly and placed at Coast Guard stations during the winter of 1967-68 at St. Joseph, Muskegon, and Manistee, Michigan; Two Rivers, and Milwaukee, Wisconsin; and Chicago, Illinois, to determine the daily integrals of solar radiation incident upon the whole lake basin. Unfortunately, due to component quality control problems and to the inexperience of the operators at some stations, not enough solar radiation data were obtained to be useful for a thermal study.

Daily air temperature records were examined for Milwaukee, Muskegon, Two Rivers, Manistee, Chicago, and Benton Harbor. The average between the daily high and low temperatures was calculated and converted to temperatures

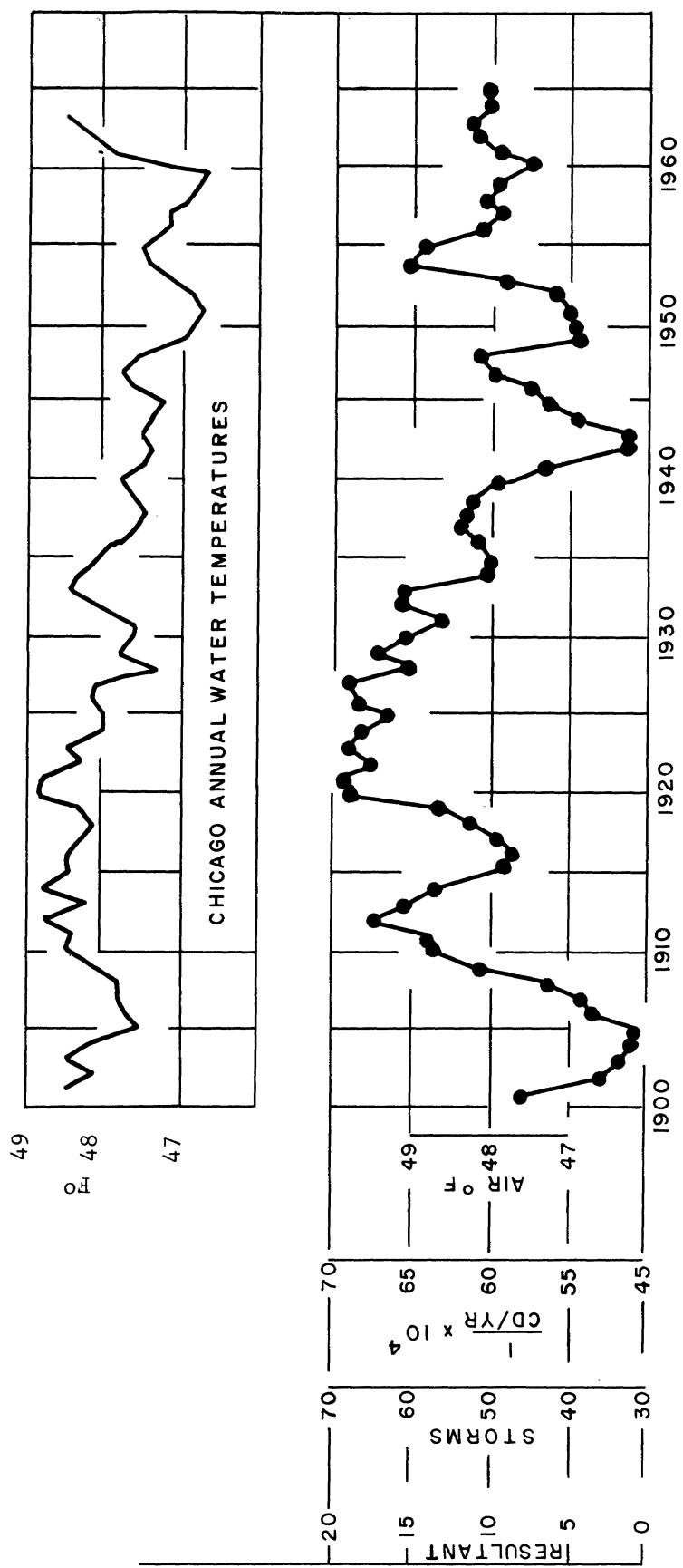


Fig. 1. Climatological predictor curve for Lake Michigan water temperature trends. After the method of Ayers (1965).

expressed in degrees Celsius. Since the freezing point is 0°C, negative values indicate freezing exposure, and positive values indicate thawing exposure. October 1 was arbitrarily defined as the beginning of the winter season, and the daily average temperatures were cumulatively summed. Since the average daily air temperature was above freezing during the month of October, the cumulative degree-day curve increases to a maximum that occurs at the onset of freezing weather. The negative degree-days that are indicative of freezing weather are subtracted from the previous cumulative total. The cumulative curve reaches a minimum and starts to increase again with the onset of warm spring weather in April. The date of the maximum of the cumulative degree-day curve indicated the onset of freezing weather, and therefore, of the freeze-up date. Figure 2 gives the cumulative degree-day curve for Milwaukee for the winter seasons of 1962-63 through 1967-68. The difference between the maximum and minimum values of the cumulative degree-day curve is a measure of the severity (freezing exposure) of the winter season. It is seen that the curve maximum occurs at dates varying from 25 November to 16 December, and that the curve minima occur between 2 March and 31 March. Freezing weather begins at the time of the curve maximum, and thawing weather at the time of the curve minimum. The dates of the maxima and minima of the curves are indicators of the freeze-up and break-up dates, respectively. Of course, accurate measurements of the solar radiation must be considered to obtain a precise prediction of the freeze-up and break-up dates.

Table 2 summarizes the cumulative degree-day data for three pairs of weather stations for the winter seasons of 1962-63 through 1963-64. The station pairs, Two Rivers - Manistee, Milwaukee - Muskegon, and Chicago - Benton Harbor were selected to be representative of the northern, middle, and southern portions of the lake basin. The dates and the cumulative degree-day values are given for each of the station records. The algebraic difference between the maximum and minimum values is the freezing exposure for each of the records. The Milwaukee records show that the severity of the winter seasons varied from 866 degree-days of freezing exposure in 1962-63 (the record ice year) to 439 during 1967-68. The very low freezing exposure during 1967-68 explains why, in spite of an ice potential index that indicated a possibility of extremely heavy ice cover, relatively little ice was formed as compared with the record year of 1962-63. On the other hand, the heavy ice potential index explains the persistence of the late-winter ice long into the spring of the year.

For the six stations considered, the winter freezing exposure ranged from 192 to 866 Celsius degree-days during the six winter seasons under study. The summer (7 April to 1 October) heating period showed approximately 3000 Celsius degree-days for all station records. The data for freezing exposure and heating (thawing) exposure are to be considered only as exposure indices, and cannot be construed as direct indicators of heat flux. For example, Table 3 gives the significant points for the cumulative degree-day curves from 6 April 1962 through 7 April 1968. The date points given are the beginning of the defined summer period, 7 April, the beginning of the defined winter period, 1 October, and the dates of the winter maxima and minima, approximately 10 December and 10 March, respectively. These data indicate a cumulative annual heating exposure of approximately 3000 Celsius degree-days.

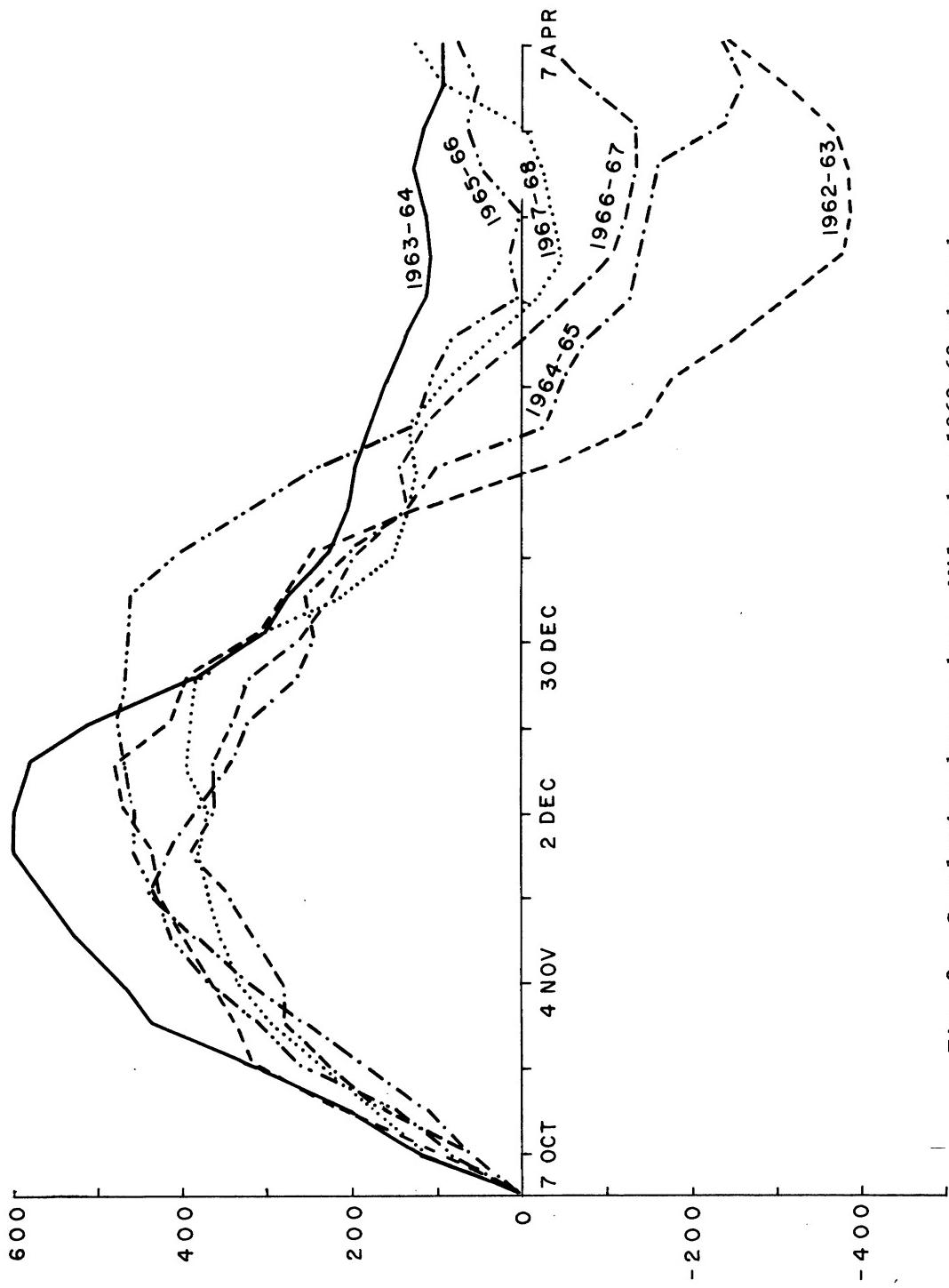


Fig. 2. Cumulative degree-days, Milwaukee 1962-63 through 1967-68.

Table 2. Summary of cumulative degree-day data and freezing exposure for six winter seasons 1962-63 through 1967-68.

TWO RIVERS - MANISTEE

	Two Rivers				Manistee							
	Max		Min		Freezing Exposure		Max		Min		Freezing Exposure	
1962-1963	464	Dec 9	-376	Mar 24	840		521	Dec 9	-194	Mar 24	615	
1963-1964	578	Nov 25	166	Mar 31	412		638	Dec 2	292	Mar 31	346	
1964-1965	411	Nov 18	-256	Mar 31	667		512	Nov 18	67	Mar 31	445	
1965-1966	428	Dec 16	- 24	Mar 10	452		497	Dec 16	191	Feb 24	306	
1966-1967	355	Nov 25	-169	Mar 24	524		422	Nov 25	67	Mar 24	355	
1967-1968	330	Nov 25	-195	Mar 2	525		423	Dec 23	- 4	Mar 16	427	

MILWAUKEE - MUSKEGON

	Milwaukee				Muskegon							
	Max		Min		Freezing Exposure		Max		Min		Freezing Exposure	
1962-1963	479	Dec 9	-387	Mar 10	866		514	Dec 9	-131	Mar 17	645	
1963-1964	599	Nov 25	92	Mar 31	507		652	Dec 2	395	Feb 24	257	
1964-1965	437	Nov 18	-259	Mar 31	696		455	Nov 25	115	Mar 31	340	
1965-1966	478	Dec 16	6	Mar 10	472		512	Dec 16	171	Feb 24	341	
1966-1967	389	Nov 25	-134	Mar 17	523		439	Dec 9	124	Mar 24	315	
1967-1968	393	Dec 9	- 46	Dec 9	439		444	Dec 23	70	Mar 2	379	

CHICAGO - BENTON HARBOR

	Chicago				Benton Harbor							
	Max		Min		Freezing Exposure		Max		Min		Freezing Exposure	
1962-1963	680	Dec 9	121	Mar 24	559		597	Dec 9	41	Mar 3	556	
1963-1964	803	Dec 2	524	Mar 3	279		714	Dec 9	522	Feb 24	192	
1964-1965	612	Nov 18	268	Mar 31	344		569	Nov 18	314	Mar 31	255	
1965-1966	707	Jan 6	419	Feb 24	288		726	Jan 6	519	Feb 24	207	
1966-1967	521	Nov 25	206	Mar 10	315		378	Dec 9	108	Mar 10	270	
1967-1968	498	Dec 23	178	Mar 2	320		499	Dec 23	204	Mar 2	295	

Table 3. Cumulative Celsius degree-days, Milwaukee, Chicago, Two Rivers  
1962-1968.

	Milwaukee			Chicago			Two Rivers	
1962	6 Apr.	0	1962	6 Apr.	0	1962	6 Apr.	0
	1 Oct.	2856		1 Oct.	3372		1 Oct.	2636
	9 Dec.	3335		9 Dec.	4052		9 Dec.	3100
1963	10 May	2469	1963	24 Mar.	3493	1963	24 Mar.	2260
	7 Apr.	2608		7 Apr.	3735		7 Apr.	2372
	1 Oct.	5441		1 Oct.	7216		1 Oct.	4984
	25 Nov.	6040		2 Dec.	8019		25 Nov.	5562
1964	31 May	5533	1964	3 May	7740	1964	31 Mar.	5150
	7 Apr.	5539		7 Apr.	7835		7 Apr.	5291
	1 Oct.	8617		1 Oct.	11260		1 Oct.	7995
	18 Nov.	9054		18 Nov.	11872		18 Nov.	8406
1965	31 Mar.	8358	1965	31 Mar.	11528	1965	31 Mar.	7739
	7 Apr.	8386		7 Apr.	11562		7 Apr.	7751
	1 Oct.	11240		1 Oct.	14726		1 Oct.	10276
	16 Dec.	11718		6 Jan.	15433		16 Dec.	10704
1966	10 Mar.	11246		24 Feb.	15145	1966	10 Mar.	10252
	7 Apr.	11316		7 Apr.	15287		7 Apr.	10307
	1 Oct.	14143		1 Oct.	18496		1 Oct.	12964
	25 Nov.	14532		25 Nov.	19017		25 Nov.	13319
1967	17 Mar.	14009	1967	10 Mar.	18702	1967	24 Mar.	12795
	7 Apr.	14117		7 Apr.	19373		7 Apr.	12878
	1 Oct.	16884		1 Oct.	22374		1 Oct.	15302
	9 Dec.	17277		23 Dec.	22872		25 Nov.	15632
1968	2 Mar.	16838	1968	2 Mar.	22552	1968	2 Mar.	15107
	7 Apr.	17011		7 Apr.	22796		7 Apr.	15189

The pattern of sensible heat transfer from the water mass to the atmosphere of the lake may be demonstrated by taking differences between the cumulative degree-day curves for cross-lake station pairs. Figure 3 gives the cross-lake difference for the northern pair of stations, Two Rivers and Manistee. Through the period of study, the apparent loss of heat to the atmosphere from the water mass as the air crosses the lake from Two Rivers to Manistee is equivalent to approximately 150 degree-days, between 1 October and 3 February as determined from air temperature measurements. This indication cannot be interpreted in terms of a heat flux until wind data are considered and the volume of warmed air mass is determined. After 3 February, the pattern of heat transfer becomes less distinct. The cross-lake warming of the air mass between Milwaukee and Muskegon is shown by the degree-day differences in Figure 4. For the winter seasons of 1962-63, 63-64, 64-65, and 66-67, the cross-lake increases were very similar (250 degree-days by 3 March), through a range of Milwaukee freezing exposures of 507 to 866 degree-days. For the two seasons of mild winters 1965-66 and 67-68 (with freezing exposures of 472 and 439 degree-days) the cross-lake warming was reduced to 150 cumulative degree-days over the same period. Figure 5, showing the cross-lake differences for Chicago and Benton Harbor, shows no regular pattern of cross-lake heat exchange. In this case, it is suggested that the data might be biased by the southern locations of the stations, inasmuch as southwesterly winds do not have representative over-water trajectories between Chicago and Benton Harbor.

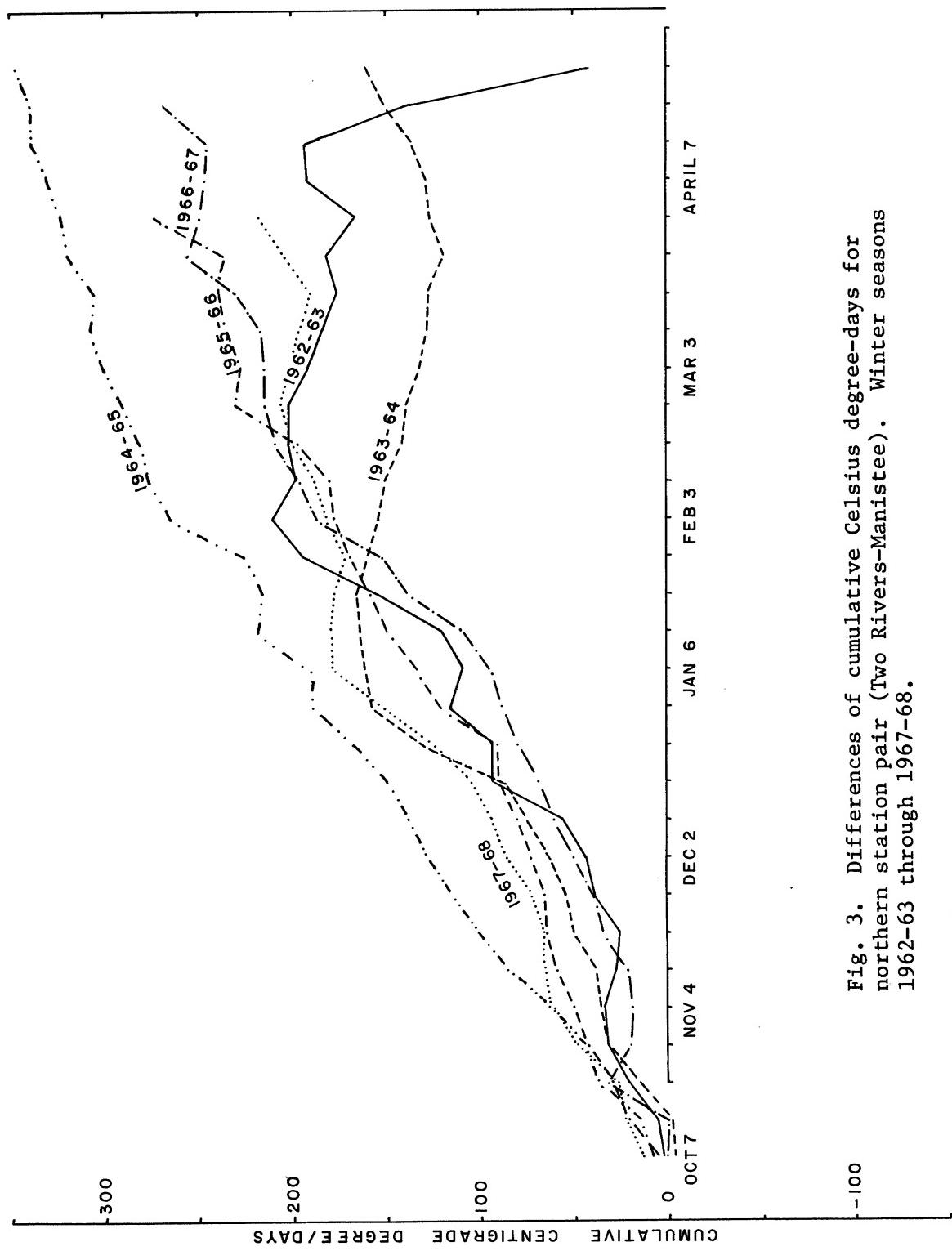


Fig. 3. Differences of cumulative Celsius degree-days for northern station pair (Two Rivers-Manistee). Winter seasons 1962-63 through 1967-68.

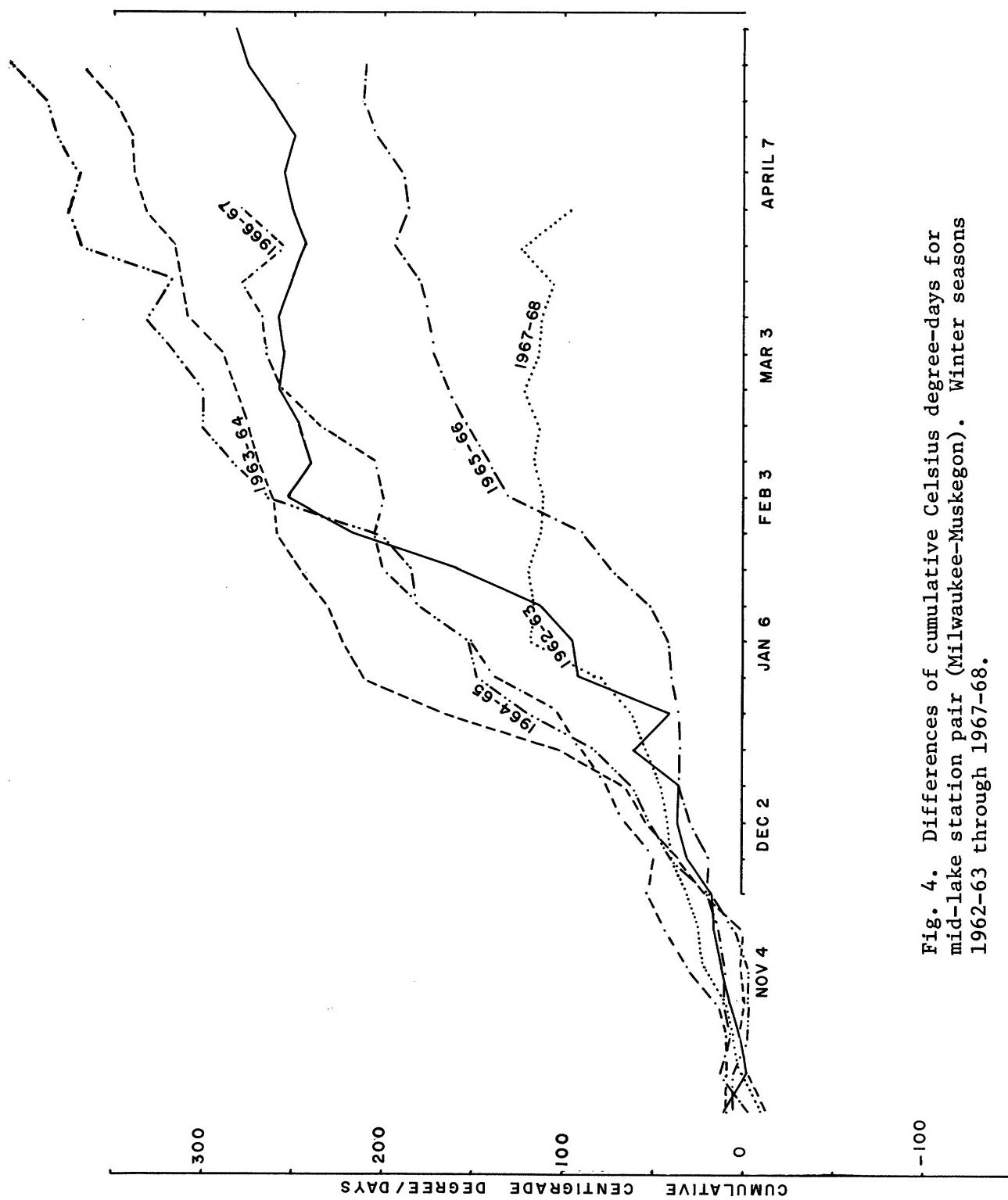


Fig. 4. Differences of cumulative Celsius degree-days for mid-lake station pair (Milwaukee-Muskegon). Winter seasons 1962-63 through 1967-68.

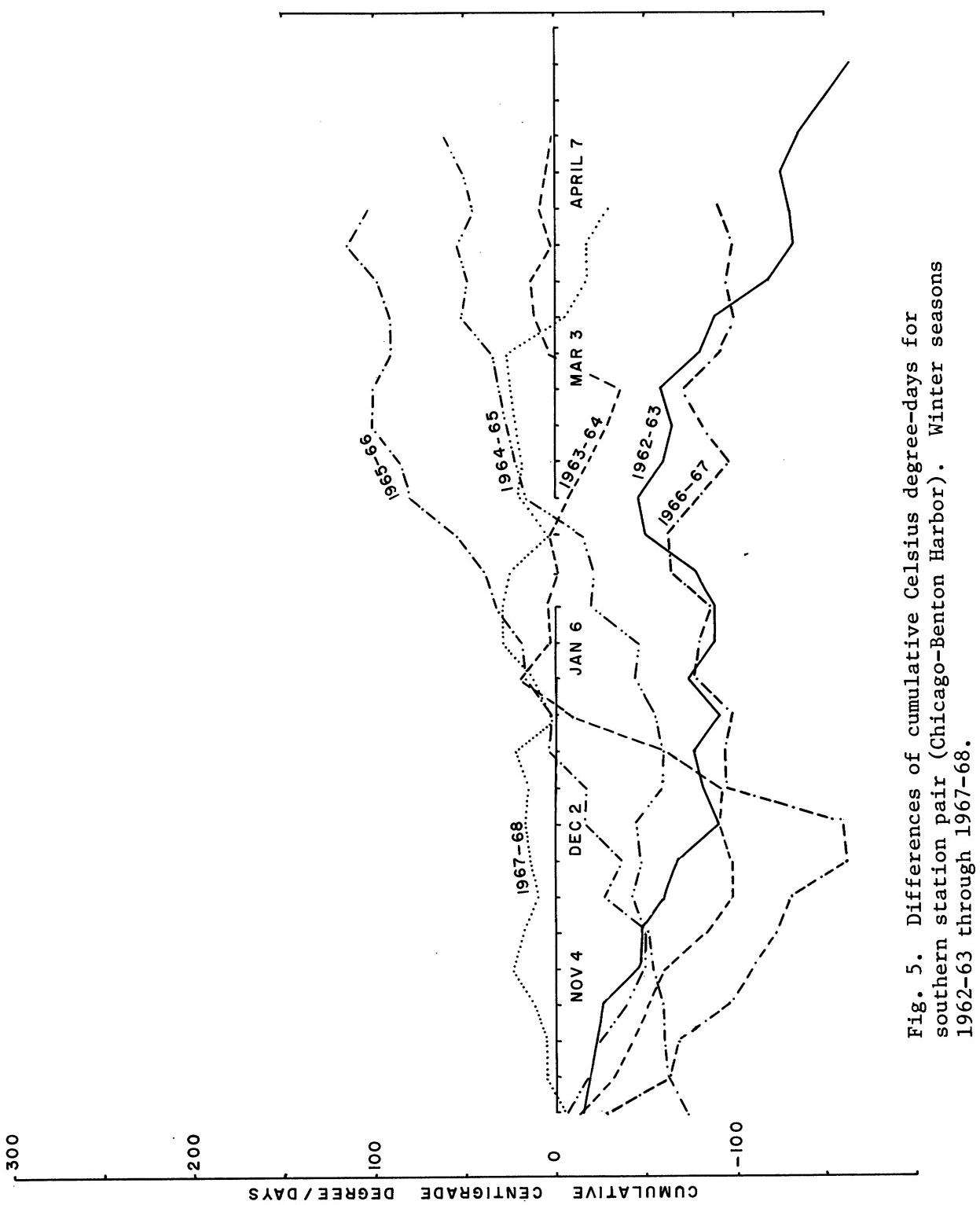


Fig. 5. Differences of cumulative Celsius degree-days for southern station pair (Chicago-Benton Harbor). Winter seasons 1962-63 through 1967-68.

## RECOMMENDATIONS

The feasibility of using early-winter water temperature data as an ice potential index has been demonstrated. Following a method similar to that of Richards (1964), it has been shown that freezing exposure data may be developed to provide short-term predictions of freeze-up and break-up dates. Ayers' climatological calculations provide a potential means for indicating water temperature trends five years in advance. It is now possible to begin operational application of the above techniques, and to implement concentrated measurements programs to provide the necessary data for precise studies of the annual thermal budget of the lake.

As suggested in a previous section of this report, all Coast Guard cutters should be instrumented with precision thermistor bridges for the measurement of intake water temperatures. Water temperature measurements should be made hourly during the fall runs to recover the aids to navigation. Additional cruises should be scheduled every three weeks during the winter season to obtain representative deep-water temperatures from the lake.

Routine flights should be scheduled on a two-week basis for mapping of the total ice cover on the lake by both trained ice observers and using aerial photography as necessary. This program could be implemented by the Coast Guard in cooperation with the U.S. Lake Survey.

An operational program should be established for the collection and maintenance of a continuous record of ice cover, winter water temperature data, and freezing exposure data at Coast Guard or Weather Bureau headquarters in Cleveland. Appropriate atlases should be compiled and maintained for future refinement of the operational prediction techniques.

A cooperative program should be established between the Coast Guard, Weather Bureau and Lake Survey to establish solar radiation instrumentation at Coast Guard stations around the basin of the lake, to provide data necessary for accurate prediction of the break-up date.

Full support should be given to a research program in connection with the International Field Year Great Lakes to provide two full years of concentrated study of the thermal budget of a Great Lake (Lake Ontario). Two years of data will be necessary to accurately interpret the relationship between the lake temperature structure and the various energy exchanges with the air mass, radiant energy exchange, evaporation and precipitation, and ground-water and run-off heat exchanges. A minimum of two years of full data will be necessary to establish the dynamics of the thermal budget of the lake because of the heat storage in the water mass of the lake from season to season.

#### APPENDIX A: LAKE MORPHOLOGY

Winter temperature data have been reduced and analyzed from the U.S. Public Health Service/Federal Water Pollution Control Administration buoy stations established in Lake Michigan during the winter seasons of 1962-63 and 1963-64. The 90-minute temperature readings from each of the 96 thermograph records have been published as Special Report No. 39, Great Lakes Research Division (Noble and Michaelis 1968). The weekly average temperatures from these records have been published in the earlier report by Heap and Noble (1966). Recording thermographs were placed at 24 stations in the basin of Lake Michigan at depths of 10, 15, 22, 30, 60, 90, and each successive 30-meter level to the bottom of the lake. For completeness, and for future use in the computation of heat storage in the lake basin during the winter months, the volumes of successive depth-layers have been computed, using the standard thermograph station depths as centers for the depth layers. The depth-layers so selected were 0-45 ft, 45-67.5 ft, 67.5-87.5 ft, 87.5-150 ft, 250-350 ft, 350-450 ft, etc. The areas of the top and bottom surfaces of the depth layers were computed in terms of square miles, and the depths in feet. Accordingly the volume elements given in Table A, are expressed in units of [mile<sup>2</sup> ft].

Table A. Depth-layer volumes for Lake Michigan. Layer surfaces in units of square miles, depths in feet. Layer volumes expressed in units of [mile<sup>2</sup> ft].

Layer [ft]	Layer Volume L. Michigan including Green Bay & Traverse Bay, [mile <sup>2</sup> ft]	Layer Volume Green Bay [mile <sup>2</sup> ft]	Layer Volume Traverse Bay [mile <sup>2</sup> ft]
0-45	935,131.6	58,175.3	11,381.4
45-67.5	432,671.4	17,850.8	4,468.2
67.5-87.5	357,621.4	9,367.9	3,516.8
87.5-150	1,002,675.8	2,860.0	8,895.9
150-250	1,331,181.6		9,231.4
250-350	988,858.3		4,975.3
350-450	567,817.6		1,812.2
450-550	321,861.0		319.9
550-650	180,948.4		
650-750	101,870.6		
750-850	38,810.2		
850-950	1,694.5		

## APPENDIX B: TEMPERATURE STRUCTURE OF LAKE MICHIGAN

The Great Lakes Research Division has adopted the following format for BT data cards:

BT4205987170 08JU630835 0620S5005B21 000148005147007106008086010076015058021052  
BT4205987170 08JU630835 0620S5005B22 033048054046

These two cards are typical of those used for BT casts. The water temperature is read at the water surface, and at each depth where there is a discontinuity in the temperature curve. These two cards are coded "BT" to designate the data card type. The data are from latitude  $42^{\circ}05.9'N$ ,  $87^{\circ}17.0'W$ , for 8 June 1963 at 0835 EST. The data are for BT cast number 0620 from the INLAND SEAS. The BT serial number is 5005B. Two data cards are needed to report the cast data, and the cards shown above are cards numbers 1 and 2 for the given cast, respectively. The first card shows a surface temperature reading of  $14.8^{\circ}C$ . The following data on the cards are coded as (ddd TTT), where ddd is the depth to the nearest whole meter, and TTT is the temperature to the nearest  $0.1^{\circ}C$ . The final reading on the second card shows a temperature of  $4.6^{\circ}C$  at 54 meters. The following program was developed to compute the average temperature for each 10-m layer of water depth for each one-degree square of latitude and longitude for each month of the year.

# TEMPERATURE AVERAGES PROGRAM

```

C THIS IS A PROGRAM FOR TEMPERATURE AVERAGES OF EVERY 10 M. DEPTH.
0001  INTEGER DEPTH,YR,SLNO,C,BAD,P(I),IX(30,12),BT//BT//MONTH(12)/
      1'JA', 'FE', 'MA', 'AP', 'MY', 'JU', 'AU', 'SP', 'OC', 'NO', 'DC'
0002  REAL A(30,12),S(300),T(10),SM(30),TEMP(12)
0003  1 CALL REWIND(7)
0004  LSLN=0
0005  LCDNO=0
0006  Z READ(5,100,END=10) ID,LT,LN,MON,YR,SLNO,N,C,(P(I),T(I),I=1,7) -
100   (P(I),T(I),A2,I,12,T9,12,117,A2,T19,12,T27,13,T36,11,11,T39,7(I3,
      1F3,0))
0008  IF(ID,NE,BT) GO TO 2
0009  IF(NLT,C,OR((C,EQ,1,AND,SLNO,EO,LSLN)) GO TO 3
0010  IF(C,GT,1,AND,SLNO,NE,LSLN) GO TO 3
0011  IF(C,NE,(LCDNO+1)) GO TO 3
0012  LCDNO=
0013  GO TO 4
0014  3 WRITE(6,101)
0015  101 FORMAT('0',T20,'CARDS NOT IN ORDER')
0016  WRITE(6,103)SLNO,MON,YR,N,C
0017  103 FORMAT(120,13,5X,A2,5X,12,5X,11,5X,11)
0018  LSLN=
0019  4 IF(C,EO,NS) LCDNO=
0020  IF(N,GE,C) LSLN=SLNO
0021  WRITE(7,102) ID,LT,LN,MON,YR,SLNO,N,C,(P(I),T(I),I=1,7)
0022  102 FORMAT(12,A2,12,3X,12,6X,A2,12,6X,13,6X,11,11,(T39,7(I3,F4.0)))
0023  GO TO 2
0024  10 CALL REWIND(7)
0025  DO 50 LDN=85, 87
0026  DO 50 LAT=41, 45
0027  DO 11 K=1, 12
0028  DO 11 I=1, 30
0029  AI,VI=0.0
0030  IX,I=0
0031  11 CONTINUE
0032  9 DO 12 K=1, 300
0033  SKK=0.0
0034  12 CONTINUE
0035  13 DO 14 K=1, 30
0036  SM(K)=0.0
0037  14 CONTINUE
0038  LDEP=1
0039  INK=0
0040  15 DO 16 K=1, 8
0041  P(I)=0
0042  K=K+1
0043  16 CONTINUE
0044  18 READ(7,102,END=39) ID,LT,LN,MON,YR,SLNO,N,C,(P(I),T(I), I=1, 7)
0045  IF(LT,NE,LAT,OR,LT,NE,LCN,OR,LT,NE,BT) GO TO 15
0046  DO 19 IM=1, 12
0047  IF(MON,EO,MONTH(IM)) GO TO 20
0048  19 CONTINUE
0049  20 M=IM
0050  DO 21 I=1, 8
0051  IF(T(I),EQ,0.0) GO TO 15
0052  IF(T(L),EQ,0.0) GO TO 22
0053  21 CONTINUE
0054  22 DO 23 I=1, IN
0055  DEPTH=P(I)+1
0056  S(DEPTH)=T(I)
0057  23 CONTINUE
0058  K=LDEP
0059  24 IND=P(IN)+1
0060  KD=K
0061  DO 25 K=K, IND
0062  IF(K,EQ,KD,OR,K,LE,INK) GO TO 25
0063  IF(S(K)-SKK,NE,0.0) GO TO 27
0064  25 SKK=S(KD)-(KD-Q)
0065  27 Q=(SKK-SKK)/(K-KD)
0066  DO 29 J=KD, K
0067  JN=J-KD
0068  SJ(J)=SKK-(JN*Q)
0069  29 CONTINUE
0070  31 IF(K,EQ,IND) GO TO 31
0071  GO TO 24
0072  31 I=LDEP
0073  31 JND=IND-10
0074  DO 32 I=1, JND, 10
0075  IX(I)=0/I/10
0076  SM(I)=0
0077  DO 33 K=1, 9
0078  DO 33 K=1, 9
0079  SM(J)=SI(K)+SM(J)
0080  33 CONTINUE
0081  AI,J,M)=(I,J,M)+SM(J)/10.
0082  IX(J,M)=IX(I,J,M)+1
0083  35 CONTINUE
0084  IF(N,C) 36, 36, 37
0085  36 GO TO 9
0086  37 LDEP=(IND/10)*10+1
0087  INK=IND
0088  GO TO 15
0089  39 CALL REWIND(7)
0090  WRITE(6,105)
0091  105 FORMAT(11, T25, 'AVERAGE TEMPERATURE BY 10 M. LAYER')
0092  WRITE(6,106) LAT, LON, YR
0093  106 FORMAT('0',T23, 'LATITUDE=' ,T33,12,T36, 'N LONGITUDE=' ,T52,12,
      1T55, 'W '19, '161,12)
0094  WRITE(6,107)
0095  107 FORMAT('0',T7, 'INTERVAL JAN FEB MAR APR MAY JU
      IN JUL AUG SEP OCT NOV DEC')
0096  DO 43 I=1, 300, 10
0097  DO 43 J=1, 12, 1
0098  DEPH=I-1
0099  DEPH=DEPTH*I
0100  IF((IX(I)+10)/10,J,EQ,0) GO TO 42
0101  TEMP(J)=AI((I+10)/10,J)/(10*IX((I+10)/10,J))
0102  GO TO 43
0103  42 TEMP(J)=0.0
0104  43 CONTINUE
0105  IF(I,EQ,1,CR,I,EQ,101,OR,I,EQ,201) GO TO 44
0106  WRITE(6,108) DEPH,LDEP,(TEMP(J), J=1, 12)
0107  108 FORMAT(' ',T6,13,T10,' ',T12,13,T18,12(F4.1,3X))
0108  GO TO 45
0109  44 WRITE(6, 109) DEPTH, LDEP, (TEMP(J), J=1, 12)
0110  109 FORMAT('0',T6,13,T10,' ',T12,13,T18,12(F4.1,3X))
0111  45 CONTINUE
0112  WRITE(6,110)
0113  110 FORMAT('14, T25, 'NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE')
0114  WRITE(6,111) LAT, LON, YR
0115  111 FORMAT('0',T23, 'LATITUDE=' ,T33,12,T36, 'N LONGITUDE=' ,T52,12,
      1T60, 'W '19, '166,12)
0116  WRITE(6,107)
0117  DO 45 I=1, 300, 10
0118  DEPH=I-1
0119  DEPH=DEPTH*I
0120  IF((IX(I)+1,CR,I,EO,101,OR,I,EO,201) GO TO 47
0121  WRITE(6,113) DEPH, LDEP, ((IX((I+10)/10,J), J=1, 12)
0122  113 FORMAT(' ',T6,13,T10,' ',T12,13,T18,12(F4.1,3X))
0123  GO TO 49
0124  114 FORMAT('0',T6,13,T10,' ',T12,13,T18,12(F4.1,3X))
0125  47 WRITE(6,114) DEPH, (IX((I+10)/10,J), J=1, 12)
0126  49 CONTINUE
0127  50 CONTINUE
0128  END

```



Table B-1

AVERAGE TEMPERATURE BY 10 M. LAYER						
	LATITUDE = 45° N LONGITUDE = 85° W					
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0
100 - 109	0.0	0.0	0.0	0.0	0.0	0.0
110 - 119	0.0	0.0	0.0	0.0	0.0	0.0
120 - 129	0.0	0.0	0.0	0.0	0.0	0.0
130 - 139	0.0	0.0	0.0	0.0	0.0	0.0
140 - 149	0.0	0.0	0.0	0.0	0.0	0.0
150 - 159	0.0	0.0	0.0	0.0	0.0	0.0
160 - 169	0.0	0.0	0.0	0.0	0.0	0.0
170 - 179	0.0	0.0	0.0	0.0	0.0	0.0
180 - 189	0.0	0.0	0.0	0.0	0.0	0.0
190 - 199	0.0	0.0	0.0	0.0	0.0	0.0

AVERAGE TEMPERATURE BY 10 M. LAYER						
	LATITUDE= 42 N			LONGITUDE= 86 W		
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0

Table B-1 (Continued)

Table B-1 (Concluded)

AVERAGE TEMPERATURE BY 10 M. LAYER						
	LATITUDE= 44 N LONGITUDE= 87 W 1926					
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0

Table B-2

## AVERAGE TEMPERATURE BY 10 M. LAYER

NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE

LATITUDE= 45 N LONGITUDE=85 W 1955												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0	14.4	0.0	18.6	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0	10.8	0.0	16.4	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0	7.2	0.0	8.1	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0	5.3	0.0	5.6	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0	5.2	0.0	5.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0	5.0	0.0	4.7	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0	4.7	0.0	4.7	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	4.6	0.0	4.4	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	4.2	0.0	4.2	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	4.1	0.0	4.1	0.0	0.0	0.0
100 - 109	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
110 - 119	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
120 - 129	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
130 - 139	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
140 - 149	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
150 - 159	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
160 - 169	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
170 - 179	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
180 - 189	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
190 - 199	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

## AVERAGE TEMPERATURE BY 10 M. LAYER

NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE

LATITUDE= 41 N LONGITUDE=86 W 1955												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0	16.5	0.0	20.5	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0	10.0	0.0	12.1	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0	9.0	0.0	10.6	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0	8.0	0.0	7.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0	7.0	0.0	6.2	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0	6.0	0.0	5.5	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0	5.0	0.0	4.5	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	4.0	0.0	3.5	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	3.0	0.0	2.5	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	2.0	0.0	1.5	0.0	0.0	0.0

## AVERAGE TEMPERATURE BY 10 M. LAYER

NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE

LATITUDE= 41 N LONGITUDE=86 W 1955												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0	17.0	0.0	20.5	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0	12.4	0.0	14.0	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0	9.2	0.0	10.6	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0	7.4	0.0	6.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0	6.4	0.0	5.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0	5.7	0.0	4.5	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0	5.5	0.0	4.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	5.3	0.0	3.5	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	5.1	0.0	2.5	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	5.1	0.0	1.5	0.0	0.0	0.0
100 - 109	0.0	0.0	0.0	0.0	0.0	0.0	5.0	0.0	0.0	0.0	0.0	0.0
110 - 119	0.0	0.0	0.0	0.0	0.0	0.0	5.2	0.0	0.0	0.0	0.0	0.0
120 - 129	0.0	0.0	0.0	0.0	0.0	0.0	5.0	0.0	0.0	0.0	0.0	0.0
130 - 139	0.0	0.0	0.0	0.0	0.0	0.0	4.8	0.0	0.0	0.0	0.0	0.0
140 - 149	0.0	0.0	0.0	0.0	0.0	0.0	4.6	0.0	0.0	0.0	0.0	0.0
150 - 159	0.0	0.0	0.0	0.0	0.0	0.0	4.5	0.0	0.0	0.0	0.0	0.0
160 - 169	0.0	0.0	0.0	0.0	0.0	0.0	4.4	0.0	0.0	0.0	0.0	0.0
170 - 179	0.0	0.0	0.0	0.0	0.0	0.0	4.3	0.0	0.0	0.0	0.0	0.0
180 - 189	0.0	0.0	0.0	0.0	0.0	0.0	4.2	0.0	0.0	0.0	0.0	0.0
190 - 199	0.0	0.0	0.0	0.0	0.0	0.0	4.0	0.0	0.0	0.0	0.0	0.0

Table B-2 (Continued)

AVERAGE TEMPERATURE BY 10 M. LAYER						
	LATITUDE = 43 N LONGITUDE = 86 W 1955					
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN
0 - 9	0.0	0.0	0.0	0.0	0.0	14.2
10 - 19	0.0	0.0	0.0	0.0	0.0	14.0
20 - 29	0.0	0.0	0.0	0.0	0.0	14.0
30 - 39	0.0	0.0	0.0	0.0	0.0	14.0
40 - 49	0.0	0.0	0.0	0.0	0.0	14.0
50 - 59	0.0	0.0	0.0	0.0	0.0	14.0
60 - 69	0.0	0.0	0.0	0.0	0.0	14.0
70 - 79	0.0	0.0	0.0	0.0	0.0	14.0
80 - 89	0.0	0.0	0.0	0.0	0.0	14.0
90 - 99	0.0	0.0	0.0	0.0	0.0	14.0
100 - 109	0.0	0.0	0.0	0.0	0.0	14.0
110 - 119	0.0	0.0	0.0	0.0	0.0	14.0
120 - 129	0.0	0.0	0.0	0.0	0.0	14.0
130 - 139	0.0	0.0	0.0	0.0	0.0	14.0
140 - 149	0.0	0.0	0.0	0.0	0.0	14.0
150 - 159	0.0	0.0	0.0	0.0	0.0	14.0
160 - 169	0.0	0.0	0.0	0.0	0.0	14.0
170 - 179	0.0	0.0	0.0	0.0	0.0	14.0
180 - 189	0.0	0.0	0.0	0.0	0.0	14.0
190 - 199	0.0	0.0	0.0	0.0	0.0	14.0

### NUMBER OF BT<sup>MS</sup>'S USED TO COMPUTE AVER. TEMPERATURE

#### AVERAGE TEMPERATURE BY 10 M. LAYER

LATITUDE = 44 N LONGITUDE = 86 W 1955												LATITUDE = 44 N LONGITUDE = 86 W 1955													
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	13.0	0.0	17.8	0.0	0.0	0 - 9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10	0.0	13	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.1	0.0	12.6	0.0	0.0	10 - 19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10	0.0	13	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.3	0.0	5.3	0.0	0.0	20 - 29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9	0.0	12	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.7	0.0	4.7	0.0	0.0	30 - 39	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7	0.0	11	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.2	0.0	5.0	0.0	0.0	40 - 49	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7	0.0	11	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.0	0.0	4.7	0.0	0.0	50 - 59	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6	0.0	9	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.0	0.0	4.6	0.0	0.0	60 - 69	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7	0.0	8	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.9	0.0	4.4	0.0	0.0	70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7	0.0	8	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.9	0.0	4.4	0.0	0.0	80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7	0.0	8	0.0	0.0
90 - 99	C.0	3.8	0.0	4.3	0.0	0.0	90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7	0.0	8	0.0	0.0						
100 - 109	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.8	0.0	4.3	0.0	0.0	100 - 109	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6	0.0	8	0.0	0.0
110 - 119	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.8	0.0	4.2	0.0	0.0	110 - 119	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6	0.0	8	0.0	0.0
120 - 129	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.8	0.0	4.2	0.0	0.0	120 - 129	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6	0.0	6	0.0	0.0
130 - 139	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.8	0.0	4.2	0.0	0.0	130 - 139	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5	0.0	6	0.0	0.0
140 - 149	C.0	3.8	0.0	4.2	0.0	0.0	140 - 149	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5	0.0	6	0.0	0.0						
150 - 159	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.8	0.0	4.1	0.0	0.0	150 - 159	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5	0.0	6	0.0	0.0
160 - 165	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.7	0.0	4.0	0.0	0.0	160 - 165	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5	0.0	5	0.0	0.0
170 - 179	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.7	0.0	4.0	0.0	0.0	170 - 179	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5	0.0	5	0.0	0.0
180 - 189	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.7	0.0	3.9	0.0	0.0	180 - 189	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5	0.0	5	0.0	0.0
190 - 199	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.7	0.0	3.9	0.0	0.0	190 - 199	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5	0.0	4	0.0	0.0
200 - 209	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.7	0.0	3.9	0.0	0.0	200 - 209	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5	0.0	4	0.0	0.0
210 - 219	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	3.7	0.0	0.0	210 - 219	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4	0.0	3	0.0	0.0
220 - 229	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	3.7	0.0	0.0	220 - 229	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2	0.0	1	0.0	0.0
230 - 239	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	3.8	0.0	0.0	230 - 239	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2	0.0	0	0.0	0.0
240 - 249	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	3.8	0.0	0.0	240 - 249	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2	0.0	0	0.0	0.0
250 - 259	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	3.8	0.0	0.0	250 - 259	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2	0.0	0	0.0	0.0
260 - 269	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	3.8	0.0	0.0	260 - 269	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2	0.0	0	0.0	0.0
270 - 279	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	3.8	0.0	0.0	270 - 279	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2	0.0	0	0.0	0.0
280 - 289	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	3.8	0.0	0.0	280 - 289	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2	0.0	0	0.0	0.0
290 - 299	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	3.8	0.0	0.0	290 - 299	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2	0.0	0	0.0	0.0
300 - 309	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	3.8	0.0	0.0	300 - 309	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2	0.0	0	0.0	0.0

NUMBER OF ETRS USED TO COMPUTE AVER. TEMPERATURE

Table B-2 (Continued)

Table B-2 (Concluded)

Table B-3

AVERAGE TEMPERATURE BY 10 M. LAYER											1961	
	LATITUDE= 42 N			LONGITUDE= 86 W			1961					
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0	13.6	0.0	0.0	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0	12.3	0.0	0.0	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0	8.5	0.0	0.0	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0	7.8	0.0	0.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0	7.0	0.0	0.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0	6.8	0.0	0.0	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0	6.0	0.0	0.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	5.0	0.0	0.0	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	4.0	0.0	0.0	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	3.0	0.0	0.0	0.0	0.0	0.0

LATITUDE = 43 N		LONGITUDE = 66 W 1961										
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.8	0.0	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.8	0.0	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.7	0.0	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.0	0.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.0	0.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.0	0.0	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.0	0.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.0	0.0	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.0	0.0	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.0	0.0	0.0	0.0	0.0

Table B-3 (Continued)

NUMBER OF BTMS USED TO COMPUTE AVER. TEMPERATURE

**NUMBER OF BITS USED TO COMPUTE AVER. TEMPERATURE**

NUMBER OF BINS USED TO COMPUTE AVER. TEMPERATURE

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Table B-3 (Concluded)

AVERAGE TEMPERATURE BY 10 M. LAYER												
LATITUDE= 43 N LONGITUDE=87 W 1961												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	20.3	0.0	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	13.7	0.0	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.4	0.0	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.7	0.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.3	0.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

AVERAGE TEMPERATURE BY 10 M. LAYER												
LATITUDE= 44 N LONGITUDE=87 W 1961												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

AVERAGE TEMPERATURE BY 10 M. LAYER												
LATITUDE= 45 N LONGITUDE=87 W 1961												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE												
LATITUDE= 43 N LONGITUDE=87 W 1961												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0	9	0	0	0	0	0	0	0	0	0	0
10 - 19	19	29	39	49	59	69	79	89	99	0	0	0
20 - 29	29	39	49	59	69	79	89	99	0	0	0	0
30 - 39	39	49	59	69	79	89	99	0	0	0	0	0
40 - 49	49	59	69	79	89	99	0	0	0	0	0	0
50 - 59	59	69	79	89	99	0	0	0	0	0	0	0
60 - 69	69	79	89	99	0	0	0	0	0	0	0	0
70 - 79	79	89	99	0	0	0	0	0	0	0	0	0
80 - 89	89	99	0	0	0	0	0	0	0	0	0	0
90 - 99	99	0	0	0	0	0	0	0	0	0	0	0

NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE												
LATITUDE= 44 N LONGITUDE=87 W 1961												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0	9	0	0	0	0	0	0	0	0	0	0
10 - 19	19	29	39	49	59	69	79	89	99	0	0	0
20 - 29	29	39	49	59	69	79	89	99	0	0	0	0
30 - 39	39	49	59	69	79	89	99	0	0	0	0	0
40 - 49	49	59	69	79	89	99	0	0	0	0	0	0
50 - 59	59	69	79	89	99	0	0	0	0	0	0	0
60 - 69	69	79	89	99	0	0	0	0	0	0	0	0
70 - 79	79	89	99	0	0	0	0	0	0	0	0	0
80 - 89	89	99	0	0	0	0	0	0	0	0	0	0
90 - 99	99	0	0	0	0	0	0	0	0	0	0	0

NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE												
LATITUDE= 45 N LONGITUDE=87 W 1961												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0	9	0	0	0	0	0	0	0	0	0	0
10 - 19	19	29	39	49	59	69	79	89	99	0	0	0
20 - 29	29	39	49	59	69	79	89	99	0	0	0	0
30 - 39	39	49	59	69	79	89	99	0	0	0	0	0
40 - 49	49	59	69	79	89	99	0	0	0	0	0	0
50 - 59	59	69	79	89	99	0	0	0	0	0	0	0
60 - 69	69	79	89	99	0	0	0	0	0	0	0	0
70 - 79	79	89	99	0	0	0	0	0	0	0	0	0
80 - 89	89	99	0	0	0	0	0	0	0	0	0	0
90 - 99	99	0	0	0	0	0	0	0	0	0	0	0

-30-

JHCO021 STOP 0 \*\*\*\* RESTART AT LOCATION 10E342

EXECUTION TERMINATED

Table B-4

Table B-4 (Continued)

Table B-4 (Continued)

Table B-4 (Concluded)

AVERAGE TEMPERATURE BY 10 M. LAYER												NUMBER OF BTMS USED TO COMPUTE AVER. TEMPERATURE													
LATITUDE= 45 N LONGITUDE=87 W 1962												LATITUDE= 45 N LONGITUDE=87 W 1962													
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 - 9	0	0	0	0	0	0	0	0	0	0	0	0
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10 - 19	0	0	0	0	0	0	0	0	0	0	0	0
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	20 - 29	0	0	0	0	0	0	0	0	0	0	0	0
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	30 - 39	0	0	0	0	0	0	0	0	0	0	0	0
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	40 - 49	0	0	0	0	0	0	0	0	0	0	0	0
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	50 - 59	0	0	0	0	0	0	0	0	0	0	0	0
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	60 - 69	0	0	0	0	0	0	0	0	0	0	0	0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	70 - 79	0	0	0	0	0	0	0	0	0	0	0	0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	80 - 89	0	0	0	0	0	0	0	0	0	0	0	0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	90 - 99	0	0	0	0	0	0	0	0	0	0	0	0

Table B-5

AVERAGE TEMPERATURE BY 10 M. LAYER

LATITUDE = 45 N LONGITUDE=85 W 1967												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	0.0	1.9	0.0	0.0	0.0	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	1.9	0.0	0.0	0.0	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	1.9	0.0	0.0	0.0	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	1.9	0.0	0.0	0.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	1.9	0.0	0.0	0.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	1.9	0.0	0.0	0.0	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	1.9	0.0	0.0	0.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

AVERAGE TEMPERATURE BY 10 M. LAYER

LATITUDE = 45 N LONGITUDE=86 W 1967												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	0.0	7.0	0.0	0.0	0.0	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	6.1	0.0	0.0	0.0	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	5.4	0.0	0.0	0.0	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	5.3	0.0	0.0	0.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	4.5	0.0	0.0	0.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	3.8	0.0	0.0	0.0	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	3.8	0.0	0.0	0.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE

LATITUDE = 45 N LONGITUDE=85 W 1967												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0	9	0	0	0	0	0	0	0	4	0	0
10 - 19	10	19	0	0	0	0	0	0	0	3	0	0
20 - 29	20	29	0	0	0	0	0	0	0	3	0	0
30 - 39	30	39	0	0	0	0	0	0	0	3	0	0
40 - 49	40	49	0	0	0	0	0	0	0	2	0	0
50 - 59	50	59	0	0	0	0	0	0	0	1	0	0
60 - 69	60	69	0	0	0	0	0	0	0	1	0	0
70 - 79	70	79	0	0	0	0	0	0	0	0	0	0
80 - 89	80	89	0	0	0	0	0	0	0	0	0	0
90 - 99	90	99	0	0	0	0	0	0	0	0	0	0

AVERAGE TEMPERATURE BY 10 M. LAYER

LATITUDE = 42 N LONGITUDE=86 W 1967												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0	9	0	0	0	15.4	10.1	0.0	0	5	8	2
10 - 19	10	19	0	0	0	11.8	10.1	0.0	0	4	8	4
20 - 29	20	29	0	0	0	7.0	10.3	0.0	0	6	6	3
30 - 39	30	39	0	0	0	5.2	10.0	0.0	0	4	9	5
40 - 49	40	49	0	0	0	4.7	7.7	0.0	0	3	4	2
50 - 59	50	59	0	0	0	4.5	5.7	0.0	0	2	4	0
60 - 69	60	69	0	0	0	4.6	4.6	0.0	0	2	3	1
70 - 79	70	79	0	0	0	4.3	4.4	0.0	0	2	2	1
80 - 89	80	89	0	0	0	4.4	4.4	0.0	0	2	2	0
90 - 99	90	99	0	0	0	4.3	0.0	0.0	0	1	2	0

NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE

LATITUDE = 42 N LONGITUDE=86 W 1967												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0	9	0	0	0	0	0	0	0	2	1	0
10 - 19	10	19	0	0	0	0	0	0	0	1	0	0
20 - 29	120	129	0	0	0	0	0	0	0	1	0	0
30 - 39	130	139	0	0	0	0	0	0	0	1	0	0
40 - 49	140	149	0	0	0	0	0	0	0	1	0	0
50 - 59	150	159	0	0	0	0	0	0	0	0	0	0
60 - 69	160	169	0	0	0	0	0	0	0	0	0	0
70 - 79	170	179	0	0	0	0	0	0	0	0	0	0
80 - 89	180	189	0	0	0	0	0	0	0	0	0	0
90 - 99	190	199	0	0	0	0	0	0	0	0	0	0

Table B-5 (Continued)

AVERAGE TEMPERATURE BY 10 M. LAYER												
LATITUDE= 43 N LONGITUDE=86 W 1967												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	1.2	0.0	0.0	5.4	6.9	14.6	0.0	0.0	0.0	0.0	0.0	0.0
10 - 19	1.4	0.0	0.0	5.0	5.8	6.5	0.0	0.0	0.0	0.0	0.0	0.0
20 - 29	1.6	0.0	0.0	5.6	6.3	6.0	0.0	0.0	0.0	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	7.1	4.9	5.3	0.0	0.0	0.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	7.2	4.7	5.0	0.0	0.0	0.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	7.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	7.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	6.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	6.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	5.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE

LATITUDE= 43 N LONGITUDE=86 W 1967												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0	0	0	0	0	0	0	0	0	0	0	0
10 - 19	0	0	0	0	0	0	0	0	0	0	0	0
20 - 29	0	0	0	0	0	0	0	0	0	0	0	0
30 - 39	0	0	0	0	0	0	0	0	0	0	0	0
40 - 49	0	0	0	0	0	0	0	0	0	0	0	0
50 - 59	0	0	0	0	0	0	0	0	0	0	0	0
60 - 69	0	0	0	0	0	0	0	0	0	0	0	0
70 - 79	0	0	0	0	0	0	0	0	0	0	0	0
80 - 89	0	0	0	0	0	0	0	0	0	0	0	0
90 - 99	0	0	0	0	0	0	0	0	0	0	0	0

NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE

LATITUDE= 44 N LONGITUDE=86 W 1967												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	2.4	3.5	6.1	10.8	0.0	0.0	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	2.4	3.3	5.6	7.0	0.0	0.0	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	2.4	3.2	5.1	5.1	0.0	0.0	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	2.4	3.2	4.6	4.5	0.0	0.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	2.3	3.0	3.6	4.4	0.0	0.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	2.3	3.0	3.5	4.3	0.0	0.0	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	2.3	3.0	3.5	4.3	0.0	0.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	2.3	3.0	3.5	4.3	0.0	0.0	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	2.3	3.0	3.5	4.3	0.0	0.0	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	2.3	3.0	3.5	4.3	0.0	0.0	0.0	0.0	0.0
100 - 109	0.0	0.0	0.0	2.3	3.0	3.5	4.3	0.0	0.0	0.0	0.0	0.0
110 - 119	0.0	0.0	0.0	2.4	3.0	3.5	4.3	0.0	0.0	0.0	0.0	0.0
120 - 129	0.0	0.0	0.0	2.4	3.0	3.5	4.3	0.0	0.0	0.0	0.0	0.0
130 - 139	0.0	0.0	0.0	2.4	3.0	3.5	4.3	0.0	0.0	0.0	0.0	0.0
140 - 149	0.0	0.0	0.0	2.5	3.0	3.5	4.3	0.0	0.0	0.0	0.0	0.0
150 - 159	0.0	0.0	0.0	2.5	3.0	3.5	4.3	0.0	0.0	0.0	0.0	0.0
160 - 169	0.0	0.0	0.0	2.6	3.0	3.5	4.3	0.0	0.0	0.0	0.0	0.0
170 - 179	0.0	0.0	0.0	2.7	3.0	3.5	4.3	0.0	0.0	0.0	0.0	0.0
180 - 189	0.0	0.0	0.0	2.7	3.1	3.5	4.3	0.0	0.0	0.0	0.0	0.0
190 - 199	0.0	0.0	0.0	2.9	3.1	3.5	4.3	0.0	0.0	0.0	0.0	0.0
200 - 209	0.0	0.0	0.0	2.9	3.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
210 - 219	0.0	0.0	0.0	3.1	3.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
220 - 229	0.0	0.0	0.0	3.1	3.2	0.0	3.7	0.0	0.0	0.0	0.0	0.0
230 - 239	0.0	0.0	0.0	3.1	3.1	0.0	3.4	0.0	0.0	0.0	0.0	0.0
240 - 249	0.0	0.0	0.0	3.2	3.2	0.0	3.4	0.0	0.0	0.0	0.0	0.0
250 - 259	0.0	0.0	0.0	3.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
260 - 269	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
270 - 279	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
280 - 289	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
290 - 299	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Table B-5 (Continued)

AVERAGE TEMPERATURE BY 10 M. LAYER

LATITUDE= 45 N LONGITUDE=86 W 1967												LATITUDE= 45 N LONGITUDE=86 W 1967													
NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE												NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE													
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	16.0	0.0	0.0	0.0	0.0	0 - 9	0	0	0	0	0	0	0	0	0	0	0	
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	13.8	0.0	0.0	0.0	0.0	10 - 19	0	0	0	0	0	0	1	0	0	0	0	
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.0	0.0	0.0	0.0	0.0	20 - 29	0	0	0	0	0	0	1	0	0	0	0	
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.1	0.0	0.0	0.0	0.0	30 - 39	0	0	0	0	0	0	1	0	0	0	0	
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.0	0.0	0.0	0.0	0.0	40 - 49	0	0	0	0	0	0	1	0	0	0	0	
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.4	0.0	0.0	0.0	0.0	50 - 59	0	0	0	0	0	0	1	0	0	0	0	
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.0	0.0	0.0	0.0	0.0	60 - 69	0	0	0	0	0	0	1	0	0	0	0	
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.0	0.0	0.0	0.0	0.0	70 - 79	0	0	0	0	0	0	1	0	0	0	0	
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	0.0	0.0	0.0	0.0	80 - 89	0	0	0	0	0	0	1	0	0	0	0	
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	0.0	0.0	0.0	0.0	90 - 99	0	0	0	0	0	0	0	0	0	0	0	
100 - 109	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	0.0	0.0	0.0	0.0	100 - 109	0	0	0	0	0	0	0	0	0	0	0	
110 - 119	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	0.0	0.0	0.0	0.0	110 - 119	0	0	0	0	0	0	0	0	0	0	0	
120 - 129	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	0.0	0.0	0.0	0.0	120 - 129	0	0	0	0	0	0	0	0	0	0	0	
130 - 139	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	0.0	0.0	0.0	0.0	130 - 139	0	0	0	0	0	0	0	0	0	0	0	
140 - 149	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	0.0	0.0	0.0	0.0	140 - 149	0	0	0	0	0	0	0	0	0	0	0	
150 - 159	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	0.0	0.0	0.0	0.0	150 - 159	0	0	0	0	0	0	0	0	0	0	0	
160 - 169	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	0.0	0.0	0.0	0.0	160 - 169	0	0	0	0	0	0	0	0	0	0	0	
170 - 179	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	0.0	0.0	0.0	0.0	170 - 179	0	0	0	0	0	0	0	0	0	0	0	
180 - 189	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	0.0	0.0	0.0	0.0	180 - 189	0	0	0	0	0	0	0	0	0	0	0	
190 - 199	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	0.0	0.0	0.0	0.0	190 - 199	0	0	0	0	0	0	0	0	0	0	0	

AVERAGE TEMPERATURE BY 10 M. LAYER

LATITUDE= 41 N LONGITUDE=87 W 1967												LATITUDE= 41 N LONGITUDE=87 W 1967													
NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE												NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE													
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	5.0	7.4	14.5	16.4	0.0	0.0	0.0	0.0	0 - 9	0	0	0	0	0	0	2	2	0	0	0	
10 - 19	0.0	0.0	0.0	0.0	3.5	5.5	7.0	9.9	0.0	0.0	0.0	0.0	10 - 19	0	0	1	10	1	1	0	0	0	0	0	
20 - 29	0.0	0.0	0.0	0.0	3.5	5.1	6.4	10.6	0.0	0.0	0.0	0.0	20 - 29	0	0	0	0	1	1	0	0	0	0	0	
30 - 39	0.0	0.0	0.0	0.0	3.5	5.1	5.8	7.1	0.0	0.0	0.0	0.0	30 - 39	0	0	0	0	1	1	0	0	0	0	0	
40 - 49	0.0	0.0	0.0	0.0	0.0	5.0	5.0	5.0	0.0	0.0	0.0	0.0	40 - 49	0	0	0	0	0	0	1	1	0	0	0	
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	50 - 59	0	0	0	0	0	0	0	0	0	0	0	
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	60 - 69	0	0	0	0	0	0	0	0	0	0	0	
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	70 - 79	0	0	0	0	0	0	0	0	0	0	0	
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	80 - 89	0	0	0	0	0	0	0	0	0	0	0	
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	90 - 99	0	0	0	0	0	0	0	0	0	0	0	

AVERAGE TEMPERATURE BY 10 M. LAYER

LATITUDE= 41 N LONGITUDE=87 W 1967												LATITUDE= 41 N LONGITUDE=87 W 1967													
NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE												NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE													
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	2.0	2.6	4.0	10.0	16.1	0.0	0.0	0.0	11.1	4.0	0 - 9	0	0	2	3	7	4	3	0	0	0	1	
10 - 19	0.0	0.0	2.1	2.6	4.6	7.9	11.7	0.0	0.0	0.0	10.9	4.0	10 - 19	0	0	0	0	0	0	0	0	0	0	6	
20 - 29	0.0	0.0	2.2	2.6	4.3	5.6	6.3	0.0	0.0	0.0	9.4	4.2	20 - 29	0	0	2	3	6	4	3	0	0	0	3	
30 - 39	0.0	0.0	2.4	2.6	4.2	4.9	4.5	0.0	0.0	0.0	8.5	4.3	30 - 39	0	0	0	1	3	5	4	3	0	0	1	
40 - 49	0.0	0.0	2.4	2.8	4.5	4.7	4.0	0.0	0.0	0.0	5.7	4.3	40 - 49	0	0	0	1	3	5	4	3	0	0	1	
50 - 59	0.0	0.0	2.4	2.8	4.5	4.6	4.6	0.0	0.0	0.0	5.4	4.3	50 - 59	0	0	0	1	2	4	3	3	0	0	1	
60 - 69	0.0	0.0	2.5	2.8	4.5	4.6	4.6	0.0	0.0	0.0	6.0	5.9	60 - 69	0	0	0	1	2	4	3	2	0	0	3	
70 - 79	0.0	0.0	2.5	2.8	4.0	4.3	4.0	0.0	0.0	0.0	5.0	4.0	70 - 79	0	0	0	1	2	4	3	2	0	0	1	
80 - 89	0.0	0.0	2.6	2.2	4.0	4.9	3.9	0.0	0.0	0.0	5.0	4.0	80 - 89	0	0	0	1	1	2	1	1	0	0	0	
90 - 99	0.0	0.0	0.0	0.0	4.0	4.8	0.0	0.0	0.0	0.0	0.0	0.0	90 - 99	0	0	0	0	0	0	0	0	0	0	0	

Table B-5 (Concluded)

AVERAGE TEMPERATURE BY 10 M. LAYER

LATITUDE= 43 N LONGITUDE=87 W 1967												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	16.5	0.0	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.3	0.0	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.1	0.0	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.4	0.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.0	0.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.0	0.0	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.0	0.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.0	0.0	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.0	0.0	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.0	0.0	0.0	0.0	0.0

NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE

LATITUDE= 43 N LONGITUDE=87 W 1967												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0	0	0	0	0	0	0	0	0	0	0	0
10 - 19	1	0	0	0	0	0	0	19	0	0	0	0
20 - 29	2	0	0	0	0	0	0	29	0	0	0	0
30 - 39	3	0	0	0	0	0	0	39	0	0	0	0
40 - 49	4	0	0	0	0	0	0	49	0	0	0	0
50 - 59	5	0	0	0	0	0	0	59	0	0	0	0
60 - 69	6	0	0	0	0	0	0	69	0	0	0	0
70 - 79	7	0	0	0	0	0	0	79	0	0	0	0
80 - 89	8	0	0	0	0	0	0	89	0	0	0	0
90 - 99	9	0	0	0	0	0	0	99	0	0	0	0

AVERAGE TEMPERATURE BY 10 M. LAYER

LATITUDE= 44 N LONGITUDE=87 W 1967												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	3.0	3.8	5.8	13.9	0.0	0.0	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	3.0	3.8	5.2	10.2	0.0	0.0	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	3.0	3.7	5.3	9.0	0.0	0.0	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	2.0	3.2	5.2	9.7	0.0	0.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	2.0	2.5	3.1	4.2	0.0	0.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	2.0	2.5	3.1	4.2	0.0	0.0	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	2.0	2.5	3.1	4.1	0.0	0.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	2.0	2.5	3.1	4.1	0.0	0.0	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	2.0	2.5	3.1	4.1	0.0	0.0	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	2.0	2.5	3.1	4.1	0.0	0.0	0.0	0.0	0.0

NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE

LATITUDE= 44 N LONGITUDE=87 W 1967												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0	0	0	0	0	0	0	9	0	0	0	0
10 - 19	1	0	0	2.0	2.3	2.7	3.1	4.0	0.0	0.0	0.0	0.0
20 - 29	2	0	0	2.0	2.6	3.1	4.0	0.0	0.0	0.0	0.0	0.0
30 - 39	3	0	0	0	2.7	2.8	3.2	4.0	0.0	0.0	0.0	0.0
40 - 49	4	0	0	0	2.7	2.8	3.2	4.0	0.0	0.0	0.0	0.0
50 - 59	5	0	0	0	2.8	2.8	3.2	4.0	0.0	0.0	0.0	0.0
60 - 69	6	0	0	0	2.9	2.9	3.2	3.9	0.0	0.0	0.0	0.0
70 - 79	7	0	0	0	2.8	2.8	3.2	3.9	0.0	0.0	0.0	0.0
80 - 89	8	0	0	0	2.9	2.9	3.2	3.9	0.0	0.0	0.0	0.0
90 - 99	9	0	0	0	2.9	2.9	3.2	3.9	0.0	0.0	0.0	0.0

AVERAGE TEMPERATURE BY 10 M. LAYER

LATITUDE= 45 N LONGITUDE=87 W 1967												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10 - 19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
20 - 29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
30 - 39	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
40 - 49	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
50 - 59	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
60 - 69	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
70 - 79	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
80 - 89	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
90 - 99	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

NUMBER OF BT'S USED TO COMPUTE AVER. TEMPERATURE

LATITUDE= 45 N LONGITUDE=87 W 1967												
INTERVAL	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
0 - 9	0	0	0	0	0	0	0	0	0	0	0	0
10 - 19	1	0	0	19	0	0	0	0	0	0	0	0
20 - 29	2	0	0	29	0	0	0	0	0	0	0	0
30 - 39	3	0	0	39	0	0	0	0	0	0	0	0
40 - 49	4	0	0	49	0	0	0	0	0	0	0	0
50 - 59	5	0	0	59	0	0	0	0	0	0	0	0
60 - 69	6	0	0	69	0	0	0	0	0	0	0	0
70 - 79	7	0	0	79	0	0	0	0	0	0	0	0
80 - 89	8	0	0	89	0	0	0	0	0	0	0	0
90 - 99	9	0	0	99	0	0	0	0	0	0	0	0

#### APPENDIX C: LAKE MICHIGAN THERMOCLINE

The following program has been developed to objectively define the thermocline depth for individual BT casts. The program inspects each BT cast, determines the upper and lower boundary layer temperatures and depths for the thermocline, and defines the depth of maximum temperature gradient as the thermocline "mean." BT casts having only two reported readings, and casts with less than  $1.0^{\circ}\text{C}$  total temperature change are defined as isothermal. In cases of complex temperature structures, two or more boundary layers (thermocline layers) may be defined.



## **THERMOCLINE PROGRAM**

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C THIS IS A LATITUDE BY LATITUDE MONTHLY MEAN THERMOCLINE PROGRAM
0001 IMPLICIT INTEGER*4 (C,Y)
0002 INTEGER*4 SLDN
0003 INTEGER*2 MN, MO, LMON, LAT
0004 DIMENSION LD(30),LT(30),LAT(5,MON(12)),DEP(30),TEM(30),DELP(30),
     1DELT(30),THEN(5,3001),DEPTP(5,3001),THENB(5,3001),DEPB(5,3001),
     2THENH(5,3001),DEPH(5,3001),ATHMR(5,1),ATHMB(5,1),ATHMH(5,1),ADEP(5,1),
     3ADEPH(5,1),ADPH(5,1)
0005 DATA LAT/11,42,52,62,45/,*1,MON//JA*,FE*,MA*,AP*,NY*,JU*,JL*,1
     1AU*,SP*,OC*,NO*,DC/*
0006 DATA THEN/1500*0.0/,DEPTP/1500*0.0/,DEPB/1500*0.0/,
     1THEN/1500*0.0/,THENB/1500*0.0/,DEPH/1500*0.0/
0007 501 FORMAT (1T,12,I9,12,T17,A2,T19,12,T20,I4,T36,11,I1,I1,T39,14I3)
0008 502 FORMAT (T20,*CARDS NOT IN ORDER AT *T45,14)
0009 503 FORMAT (T20,*DOUBLE THERMOCLINE FOR BT *T47,14)
0010 504 FORMAT (1H0,T20,*THE SECOND THERMOCLINE AT *T47,F5.0,5X,F5.1)
0011 505 FORMAT (1H0,T20,*BT*T24,I4,T30,*THERMOCLINE DATA *)
0012 506 FORMAT (T15,*UPPER *T28,F5.0,5X,F5.1)
0013 507 FORMAT (T20,*LOWER *T28,F5.0,5X,F5.1)
0014 508 FORMAT (T20,*MANY BT'S T25,14,T30,*IS AN ISOTHERMAL BT *)
0015 509 FORMAT (T20,*BT*T25,14,T30,*IS AN ISOTHERMAL BT *)
0016 510 FORMAT (1H1,T15,*TOTAL BT FOR *T30,A2,T35,I2,T40,*IS*,T45,13)
0017 511 FORMAT (T15,*AVERAGE THERMOCLINE DATA FOLLOW*)
0018 512 FORMAT (T15,*LATITUDE 4*T25,11,T28,*NUMBER OF BT *T42,I3)
0019 513 FORMAT (T15,*DISCONTINUITY LAYER, UPPER: *T45,F5.0,5X,F5.1)
0020 514 FORMAT (T35,*LOWER, T45,F5.0,5X,F5.1)
0021 515 FORMAT (T26,*THE THERMOCLINE IS*, T45,F5.0,5X,F5.1)
0022 516 FORMAT (1I0,T25*--*--*--*--*--*--*--*--*--*--*--*--*--*--*--*)
0023 520 FORMAT (1H0,T10,*TOTAL BT FOR *T19,T26,I2,T30,*IS*,T35,13)
0024 521 FORMAT (1I0,*TOTAL ISOTHERMAL BT IS*, T33,13)
0025 550 FORMAT (T15,*ISO. OF MONTH*, T30+A2,T35,I2,T40,*IS*,T45,I3)
0026      NBT=0
0027      LSLNO=0
0028      LISO=0
0029      1 DO 1000 IM=1,12
0030      NM=0
0031      ISO=0
0032      DO 100 I=1, 5
0033      NLII=0
0034      IF (IM,EQ,1) GO TO 2
0035      IF ((MON(1)).EQ.(LMON)) GO TO 5
0036      GO TO 50
0037      2 DO 101 I=1, 30
0038      LDI(I)=0
0039      LDT(I)=0
0040      DELP(I)=0.0
0041      101 DELT(I)=0.0
0042      LCN=0
0043      3 J=1+7*LCN
0044      K=7+7*LCN
0045      4 READ (5+DL,END=50) LT,LN,MO,YR,SLNO,NC,CN,(LD(I),LT(I)),I=J,K
0046      IF (NC.EQ.CN) NBT=NBT+1
0047      IF ((MON(1)).EQ.(MO)) GO TO 5
0048      GO TO 50
0049      5 GO TO 50
0050      6 IF (LSLNO.NE.SLNO.AND.NC.EQ.CN) GO TO 7
0051      6 LCN=LCN+1
0052      IF (LCN.EQ.CN) GO TO 3
0053      WRITE(6,502) SLNO
0054      GO TO 502
0055      7 LSLNO=SLNO
0056      NM=NM+1
0057      DO 8 L=1, 5
0058      IF ((LAT(L)).EQ.LT) GO TO 9
0059      8 CONTINUE
0060      9 NM=NM+1
0061      NL(N)=NL(N)+1
0062      DO 10 I=1, 30
0063      IF ((LD(I)).EQ.0) GO TO 11
0064      10 CONTINUE
0065      11 K=I-1
0066      IF (K,LE,3) GO TO 33
0067      DO 13 I=1, K
0068      DEPM(I)=0.0
0069      13 TEM(I)=LT(I)/IO.
0070      DO 14 I=2,I
0071      DEPM(I)=TEM(I)-TEM(I-1)
0072      IF ((DEPM(I-1).LT.0.0)) GO TO 33
0073      14 DEPM(I-1)=DEPM(I)-DEPM(I-1)
0074      N=NL(M)
0075      TDELM=0.0
0076      TDELS=0.0
0077      J=0
0078      Y=K-1
0079      DO 16 I=1, Y
0080      IF ((TDELM.GE.DELT(I))) GO TO 15
0081      TDELS=TDELM
0082      15 TDELM=TDELS
0083      TDELM=DELT(I)
0084      J=j
0085      GO TO 16
0086      15 IF ((TDELM.GE.DELT(I))) GO TO 16
0087      TDELS=DELT(I)
0088      J=j
0089      16 CONTINUE
0090      IF ((J,LE,Y.AND.TDELM.LE,1)) GO TO 33
0091      IF ((JJ,GE,J-OR,JJ-EQ,(J-1)*OR,JJ-EQ,(J-1))) GO TO 19
0092      IF ((IDELS-0.5*TDELM)) 19, 18, 18
0093      18 IDELS=0.5*TDELM
0094      DEPS=DELT(I)
0095      SDEP=DEPM(I)-5*XDEPS
0096      STEM=TEM(I)-0.5*XDELS
0097      WRITE(6,503) SLNO
0098      WRITE(6,504) SDEP, STEM
0099      19 JT=j
0100      J=j
0101      IF ((J,LE,2)) GO TO 28
0102      IF ((DEPM(I-1)-DELT(I-1))/TDELM>10.0)) 27, 27, 28
0103      27 IF ((DEPM(I-1)/DEPM(I-1)-DEP(2)).GE,.1) GO TO 28
0104      28

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0105 JT=JT-1
0106 GO TO 20
0107 28 THEM1(M,N)=TEM(I)
0108 DEPT(M,N)=DEP(I)
0109 29 JB=J
0110 21 I=J
0111 IF (I>ELP(I+1)) EO=0.0 GO TO 31
0112 IF (I>ELP(I+1)-DELT(I+1)/DEPM*10.1) 30, 30, 31
0113 30 IF (I>ELP(I+1))/DEP(I+1)-DEP(21)) .GE.=17 GO TO 31
0114 DEELM=DEALM+DELT(I+1)
0115 JB=JB+1
0116 GO TO 21
0117 31 THEM2(M,N)=TEM(I+1)
0118 DEPB(M,N)=DEP(I+1)
0119 32 I=J
0120 DELPM=DEP(JB+1)-DEP(JT)
0121 DEPTH(M,N)=DEP(I)+0.5*DELPM
0122 (DEPT(M,N),DEP(I),DEPM,DEPB(M,N),THEM1(M,N),
0123 WRITE(6,505) SLNO
0124 WRITE(6,506) DEPT(M,N), THEM1(M,N)
0125 WRITE(6,507) DEPB(M,N), THEM2(M,N)
0126 WRITE(6,508) DEPTH(M,N), THTEM(M,N)
0127 GO TO 2
0128 33 ISO=ISO+1
0129 LISO=LISO+1
0130 WRITE(6,509) SLNO
0131 NL(M)=NL(M)-1
0132 GO TO 2
0133 50 WRITE(6,510) MON(LM), YR, NM
0134 WRITE(6,550) MON(LM), YR, ISO
0135 WRITE(6,511)
0136 DO 35 M=M+5
0137 SUM1=0.0
0138 SUM2=0.0
0139 SUM3=0.0
0140 SUM4=0.0
0141 SUM5=0.0
0142 SUM6=0.0
0143 Y=NM
0144 DO 34 N=N1, Y
0145 IF (Y,EO,0) GO TO 34
0146 SUM1=SUM1+THEM1(M,N)
0147 SUM2=SUM2+THEM2(M,N)
0148 SUM3=SUM3+THTEM(M,N)
0149 SUM4=SUM4+DEPT(M,N)
0150 SUM5=SUM5+DEPB(M,N)
0151 SUM6=SUM6+DEPTH(M,N)
0152 34 CONTINUE
0153 ATHEM1(M,N)=SUM1/N
0154 ATHEM2(M,N)=SUM2/N
0155 ATHTEM(M,N)=SUM3/N
0156 ADEPT(M,N)=SUM4/N
0157 ADEPB(M,N)=SUM5/N
0158 ADEPTH(M,N)=SUM6/N
0159 WRITE(6,512) M, NL(M)

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Table C-1

<u>TOTAL BT FOR JA 54 IS 0</u>	<u>TOTAL BT FOR FE 54 IS 0</u>
<u>TOTAL BT FOR MA 54 IS 0</u>	<u>TOTAL BT FOR AP 54 IS 0</u>
<u>TOTAL BT FOR MY 54 IS 0</u>	<u>TOTAL BT FOR JU 54 IS 0</u>
<u>TOTAL BT FOR JL 54 IS 30</u>	<u>TOTAL BT FOR AU 54 IS 0</u>
<u>ISG. OF MONT JL 54 IS 1</u>	
<u>AVERAGE THERMOCLINE DATA FOLLOW</u>	
LATITUDE 41 NUMBER OF BT 0	
DISCONTINUITY LAYER, UPPER: 0.0	
LOWER: 0.0	
THE THERMOCLINE IS 0.	
LATITUDE 42 NUMBER OF BT 0	
DISCONTINUITY LAYER, UPPER: 0.0	
LOWER: 0.0	
THE THERMOCLINE IS 0.	
LATITUDE 43 NUMBER OF BT 0	
DISCONTINUITY LAYER, UPPER: 0.0	
LOWER: 0.0	
THE THERMOCLINE IS 0.	
LATITUDE 44 NUMBER OF BT 22	
DISCONTINUITY LAYER, UPPER: 11. 20.9	
LOWER: 17. 12.8	
THE THERMOCLINE IS 14. 16.9	
LATITUDE 45 NUMBER OF BT 7	
DISCONTINUITY LAYER, UPPER: 13. 19.8	
LOWER: 17. 14.1	
THE THERMOCLINE IS 15. 16.9	
<u>TOTAL BT FOR SP 54 IS 0</u>	<u>TOTAL BT FOR OC 54 IS 0</u>
<u>TOTAL BT FOR NO 54 IS 0</u>	<u>TOTAL BT FOR DC 54 IS 0</u>
	<u>TOTAL BT FOR 19-54 IS 1</u>
	<u>TOTAL ISOTHERMAL BT IS 30</u>

Table C-2

<u>TOTAL BT FOR</u>	<u>JA</u>	<u>55</u>	<u>IS</u>	<u>0</u>
<u>TOTAL BT FOR</u>	<u>MA</u>	<u>55</u>	<u>IS</u>	<u>0</u>
<u>TOTAL BT FOR</u>	<u>NY</u>	<u>55</u>	<u>IS</u>	<u>0</u>
<u>TOTAL BT FOR</u>	<u>NO</u>	<u>55</u>	<u>IS</u>	<u>0</u>
<u>TOTAL BT FOR</u>	<u>SP</u>	<u>55</u>	<u>IS</u>	<u>0</u>
<u>TOTAL BT FOR</u>	<u>JL</u>	<u>55</u>	<u>IS</u>	<u>0</u>
<u>TOTAL BT FOR</u>	<u>AU</u>	<u>55</u>	<u>IS</u>	<u>12.1</u>
ISO. OF MONTH AU	55	IS	15	
AVERAGE THERMOCLINE DATA FOLLOW				
LATITUDE 41 NUMBER OF BT	55	IS	20	
DISCONTINUITY LAYER, UPPER:	5.			
LOWER:	10.			11.7
THE THERMOCLINE IS	8.			15.7
LATITUDE 42 NUMBER OF BT	28			
DISCONTINUITY LAYER, UPPER:	7.			17.3
LOWER:	12.			11.0
THE THERMOCLINE IS	9.			13.2
LATITUDE 43 NUMBER OF BT	29			
DISCONTINUITY LAYER, UPPER:	5.			16.3
LOWER:	10.			9.4
THE THERMOCLINE IS	8.			12.9
LATITUDE 44 NUMBER OF BT	16			
DISCONTINUITY LAYER, UPPER:	5.			14.3
LOWER:	11.			8.0
THE THERMOCLINE IS	8.			11.1
LATITUDE 45 NUMBER OF BT	27			
DISCONTINUITY LAYER, UPPER:	10.			13.1
LOWER:	15.			8.8
THE THERMOCLINE IS	13.			10.9
<u>TOTAL BT FOR</u>	<u>DC</u>	<u>55</u>	<u>IS</u>	<u>0</u>
ISO. OF MONTH DC	55	IS	15	
AVERAGE THERMOCLINE DATA FOLLOW				
LATITUDE 41 NUMBER OF BT	55	IS	20	
DISCONTINUITY LAYER, UPPER:	14.			20.8
LOWER:	20.			10.7
THE THERMOCLINE IS	17.			15.8
LATITUDE 42 NUMBER OF BT	11			
DISCONTINUITY LAYER, UPPER:	12.			22.0
LOWER:	19.			12.2
THE THERMOCLINE IS	15.			17.1
LATITUDE 43 NUMBER OF BT	26			
DISCONTINUITY LAYER, UPPER:	12.			19.6
LOWER:	17.			9.1
THE THERMOCLINE IS	15.			14.3
LATITUDE 44 NUMBER OF BT	22			
DISCONTINUITY LAYER, UPPER:	9.			19.6
LOWER:	17.			9.7
THE THERMOCLINE IS	13.			14.6
<u>TOTAL BT FOR</u>	<u>ISOTHERMAL BT</u>	<u>55</u>	<u>IS</u>	<u>2.49</u>
<u>TOTAL BT FOR</u>	<u>ISOTHERMAL BT</u>	<u>IS</u>	<u>35</u>	

Table C-3

TOTAL BT FOR JA	61	IS	0	TOTAL BT FOR FE	61	IS	0
TOTAL BT FOR MA	61	IS	0	TOTAL BT FOR AP	61	IS	0
TOTAL BT FOR MY	61	IS	0	TOTAL BT FOR JU	61	IS	0
TOTAL BT FOR JL	61	IS	71	TOTAL BT FOR AU	61	IS	85
TSO. OF MONTH JL	61	IS	18	TSO. OF MONTH AU	61	IS	44
AVERAGE THERMOCLINE DATA FOLLOW				AVERAGE THERMOCLINE DATA FOLLOW			
LATITUDE 41 NUMBER OF BT	5			LATITUDE 41 NUMBER OF BT	28		
DISCONTINUITY LAYER, UPPER:	7.			DISCONTINUITY LAYER, UPPER:	5.		
LOWER:	9.			LOWER:	7.		
THE THERMOCLINE IS	8.			THE THERMOCLINE IS	6.		
LATITUDE 42 NUMBER OF BT	39			LATITUDE 42 NUMBER OF BT	5		
DISCONTINUITY LAYER, UPPER:	9.			DISCONTINUITY LAYER, UPPER:	6.		
LOWER:	13.			LOWER:	8.		
THE THERMOCLINE IS	11.			THE THERMOCLINE IS	7.		
LATITUDE 43 NUMBER OF BT	17			LATITUDE 43 NUMBER OF BT	8		
DISCONTINUITY LAYER, UPPER:	5.			DISCONTINUITY LAYER, UPPER:	10.		
LOWER:	10.			LOWER:	14.		
THE THERMOCLINE IS	8.			THE THERMOCLINE IS	12.		
LATITUDE 44 NUMBER OF BT	0			LATITUDE 44 NUMBER OF BT	0		
DISCONTINUITY LAYER, UPPER:	0.			DISCONTINUITY LAYER, UPPER:	0.		
LOWER:	0.			LOWER:	0.		
THE THERMOCLINE IS	0.			THE THERMOCLINE IS	0.		
LATITUDE 45 NUMBER OF BT	1			LATITUDE 45 NUMBER OF BT	0		
DISCONTINUITY LAYER, UPPER:	6.			DISCONTINUITY LAYER, UPPER:	0.		
LOWER:	9.			LOWER:	0.		
THE THERMOCLINE IS	7.			THE THERMOCLINE IS	0.		
TOTAL BT FOR SE	61	IS	9	TOTAL BT FOR OC	61	IS	0
TOTAL BT FOR NO	61	IS	0	TOTAL BT FOR DC	61	IS	0
				TOTAL BT FOR 19	61	IS	156
				TOTAL ISOTHERMAL BT	IS	62	

Table C-4

TOTAL BT FOR JA	62	IS	0		TOTAL BT FOR FE	62	IS	0
TOTAL BT FOR MA	62	IS	0		TOTAL BT FOR AP	62	IS	0
TOTAL BT FOR MY	62	IS	0		TOTAL BT FOR JU	62	IS	0
TOTAL BT FOR JL	62	IS	0		TOTAL BT FOR AU	62	IS	251
					ISO. OF MONTH AU	62	IS	19
					AVERAGE THERMOCLINE DATA FOLLOW			
					LATITUDE 41 NUMBER OF BT			
					DISCONTINUITY LAYER, UPPER:	13.		20.4
					LOWER	16.		14.5
					THE THERMOCLINE IS	14.		17.4
					LATITUDE 42 NUMBER OF BT	133		
					DISCONTINUITY LAYER, UPPER:	18.		18.3
					LOWER	23.		9.1
					THE THERMOCLINE IS	20.		13.7
					LATITUDE 43 NUMBER OF BT	70		
					DISCONTINUITY LAYER, UPPER:	18.		17.1
					LOWER	23.		8.2
					THE THERMOCLINE IS	21.		12.7
					LATITUDE 44 NUMBER OF BT	0		
					DISCONTINUITY LAYER, UPPER:	0.		0.0
					LOWER	0.		0.0
					THE THERMOCLINE IS	0.		0.0
					LATITUDE 45 NUMBER OF BT	0		
					DISCONTINUITY LAYER, UPPER:	0.		0.0
					LOWER	0.		0.0
					THE THERMOCLINE IS	0.		0.0
					LATITUDE 46 NUMBER OF BT	0		
					DISCONTINUITY LAYER, UPPER:	15		19
					LOWER	62	IS	4
					THE THERMOCLINE IS			
					LATITUDE 47 NUMBER OF BT	0		
					DISCONTINUITY LAYER, UPPER:	0.		0.0
					LOWER	40.		6.6
					THE THERMOCLINE IS	38.		9.1
					LATITUDE 48 NUMBER OF BT	0		
					DISCONTINUITY LAYER, UPPER:	0.		0.0
					LOWER	0.		0.0
					THE THERMOCLINE IS	0.		0.0
					LATITUDE 49 NUMBER OF BT	0		
					DISCONTINUITY LAYER, UPPER:	0.		0.0
					LOWER	0.		0.0
					THE THERMOCLINE IS	0.		0.0
					LATITUDE 50 NUMBER OF BT	0		
					DISCONTINUITY LAYER, UPPER:	0.		0.0
					LOWER	0.		0.0
					THE THERMOCLINE IS	0.		0.0
					LATITUDE 51 NUMBER OF BT	0		
					DISCONTINUITY LAYER, UPPER:	0.		0.0
					LOWER	0.		0.0
					THE THERMOCLINE IS	0.		0.0



Table C-5

TOTAL BT FOR	JA	63	IS	0
TOTAL BT FOR	MA	63	IS	0
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TOTAL BT FOR	AP	63	IS	141
TSO. OF MONTH	AP	63	IS	98
AVERAGE THERMOCLINE DATA FOLLOW				
LATITUDE 41 NUMBER OF BT	34			
DISCONTINUITY LAYER, UPPER:		6.		6.9
LOWER		11.		6.0
THE MEAN VALUE IS	9.			6.4
<hr/>				
LATITUDE 42 NUMBER OF BT	4			
DISCONTINUITY LAYER, UPPER:		8.		5.3
LOWER		18.		4.9
THE MEAN VALUE IS	13.			5.1
<hr/>				
LATITUDE 43 NUMBER OF BT	5			
DISCONTINUITY LAYER, UPPER:		0.		0.0
LOWER		0.		0.0
THE MEAN VALUE IS	0.			0.0
<hr/>				
LATITUDE 44 NUMBER OF BT	6			
DISCONTINUITY LAYER, UPPER:		0.		0.0
LOWER		0.		0.0
THE MEAN VALUE IS	0.			0.0
<hr/>				
LATITUDE 45 NUMBER OF BT	0			
DISCONTINUITY LAYER, UPPER:		0.		0.0
LOWER		0.		0.0
THE MEAN VALUE IS	0.			0.0
<hr/>				
TOTAL BT FOR	JU	63	IS	47
TSO. OF MONTH	JU	63	IS	5
AVERAGE THERMOCLINE DATA FOLLOW				
LATITUDE 41 NUMBER OF BT	1			
DISCONTINUITY LAYER, UPPER:		4.		19.1
LOWER		9.		11.6
THE MEAN VALUE IS	6.			15.3
<hr/>				
LATITUDE 42 NUMBER OF BT	3			
DISCONTINUITY LAYER, UPPER:		6.		14.0
LOWER		9.		8.4
THE MEAN VALUE IS	7.			11.2
<hr/>				
LATITUDE 43 NUMBER OF BT	38			
DISCONTINUITY LAYER, UPPER:		7.		10.5
LOWER		14.		7.4
THE MEAN VALUE IS	11.			9.0
<hr/>				
LATITUDE 44 NUMBER OF BT	0			
DISCONTINUITY LAYER, UPPER:		0.		0.0
LOWER		0.		0.0
THE MEAN VALUE IS	0.			0.0
<hr/>				
LATITUDE 45 NUMBER OF BT	0			
DISCONTINUITY LAYER, UPPER:		0.		0.0
LOWER		0.		0.0
THE MEAN VALUE IS	0.			0.0



Table C-5 (concluded)

	TOTAL BT FOR NO IS	63	IS	4	1	TOTAL BT FOR NO IS	63	IS	0
ISO. OF MONTH NO									
AVERAGE ISOMOCLINE DATA FOLLOW									
LATITUDE 41 NUMBER OF BT	0								
DISCONTINUITY LAYER, UPPER:	0.					0.0			
LOWER	0.					0.0			
THE MEAN VALUE IS	0.					0.0			
LATITUDE 42 NUMBER OF BT	2								
DISCONTINUITY LAYER, UPPER:	36.					13.1			
LOWER	42.					5.4			
THE MEAN VALUE IS	39.					9.3			
LATITUDE 43 NUMBER OF BT	1								
DISCONTINUITY LAYER, UPPER:	35.					13.5			
LOWER	4.					5.4			
THE MEAN VALUE IS	38.					9.4			
LATITUDE 44 NUMBER OF BT	0								
DISCONTINUITY LAYER, UPPER:	0.					0.0			
LOWER	0.					0.0			
THE MEAN VALUE IS	0.					0.0			
LATITUDE 45 NUMBER OF BT	0								
DISCONTINUITY LAYER, UPPER:	0.					0.0			
LOWER	0.					0.0			
THE MEAN VALUE IS	0.					0.0			
TOTAL BT FOR 19 IS 625									
TOTAL ISOTHERMAL BT IS 166									

Table C-6

TOTAL BT FOR	JY	64	IS	0
TOTAL BT FOR	MA	64	IS	C
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TOTAL BT FOR	JU	64	IS	19
TSO. OF MONTH	JY	64	IS	10
AVERAGE THERMOCLINE DATA FLOW				
LATITUDE 41 NUMBER OF BT	1			
DISCONTINUITY LAYER, UPPER:	0.			0.0
DISCONTINUITY LAYER, LOWER:	0.			0.0
THE MEAN VALUE IS	0.			0.0
<hr/>				
LATITUDE 42 NUMBER OF BT	1			
DISCONTINUITY LAYER, UPPER:	3.			8.1
DISCONTINUITY LAYER, LOWER:	6.			7.0
THE MEAN VALUE IS	5.			7.5
<hr/>				
LATITUDE 43 NUMBER OF BT	0			
DISCONTINUITY LAYER, UPPER:	0.			0.0
DISCONTINUITY LAYER, LOWER:	0.			0.0
THE MEAN VALUE IS	0.			0.0
<hr/>				
LATITUDE 44 NUMBER OF BT	0			
DISCONTINUITY LAYER, UPPER:	0.			0.0
DISCONTINUITY LAYER, LOWER:	0.			0.0
THE MEAN VALUE IS	0.			0.0
<hr/>				
TOTAL BT FOR	JU	64	IS	14.
TSO. OF MONTH	JU	64	IS	13
AVERAGE THERMOCLINE DATA FLOW				
LATITUDE 41 NUMBER OF BT	4			
DISCONTINUITY LAYER, UPPER:	11.			14.8
DISCONTINUITY LAYER, LOWER:	16.			10.3
THE MEAN VALUE IS	13.			12.8
<hr/>				
LATITUDE 42 NUMBER OF BT	22			
DISCONTINUITY LAYER, UPPER:	12.			13.4
DISCONTINUITY LAYER, LOWER:	21.			7.8
THE MEAN VALUE IS	17.			10.6
<hr/>				
LATITUDE 43 NUMBER OF BT	47			
DISCONTINUITY LAYER, UPPER:	11.			8.2
DISCONTINUITY LAYER, LOWER:	20.			6.0
THE MEAN VALUE IS	16.			7.1
<hr/>				
LATITUDE 44 NUMBER OF BT	28			
DISCONTINUITY LAYER, UPPER:	6.			8.3
DISCONTINUITY LAYER, LOWER:	13.			5.8
THE MEAN VALUE IS	10.			7.0
<hr/>				
LATITUDE 45 NUMBER OF BT	0			
DISCONTINUITY LAYER, UPPER:	0.			0.0
DISCONTINUITY LAYER, LOWER:	0.			0.0
THE MEAN VALUE IS	0.			0.0

Table C-6 (Continued)

TOTAL BT FOR	JL	64	IS	84		TOTAL BT FOR	AU	64	IS	68
ISO. OF MONTH	JL	64	IS	12		ISO. OF MONTH	AU	64	IS	4
AVERAGE THERMOCLINE DATA FOLLOW						AVERAGE THERMOCLINE DATA FOLLOW				
LATITUDE 41 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	2					LATITUDE 41 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	31			
LOWER	16°					LOWER	35°			
THE MEAN VALUE IS	19.					THE MEAN VALUE IS	11.			
LATITUDE 42 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	24					LATITUDE 42 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	15			
LOWER	12.					LOWER	21°			
THE MEAN VALUE IS	17.					THE MEAN VALUE IS	25.			
LATITUDE 43 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	41					LATITUDE 43 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	8			
LOWER	20°					LOWER	29°			
THE MEAN VALUE IS	17.					THE MEAN VALUE IS	12.1			
LATITUDE 44 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	5					LATITUDE 44 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	6			
LOWER	6.1					LOWER	15°			
THE MEAN VALUE IS	9.					THE MEAN VALUE IS	15.			
LATITUDE 45 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	0					LATITUDE 45 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	0			
LOWER	0.					LOWER	0.			
THE MEAN VALUE IS	0.					THE MEAN VALUE IS	0.			
TOTAL BT FOR	SP	64	IS	97		TOTAL BT FOR	OC	64	IS	30
ISO. OF MONTH	SP	64	IS	25		ISO. OF MONTH	OC	64	IS	8
AVERAGE THERMOCLINE DATA FOLLOW						AVERAGE THERMOCLINE DATA FOLLOW				
LATITUDE 41 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	3					LATITUDE 41 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	1			
LOWER	15.					LOWER	34°			
THE MEAN VALUE IS	27.					THE MEAN VALUE IS	31.			
LATITUDE 42 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	13					LATITUDE 42 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	2			
LOWER	22°					LOWER	27°			
THE MEAN VALUE IS	17.					THE MEAN VALUE IS	31.			
LATITUDE 43 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	3					LATITUDE 43 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	4			
LOWER	4.9					LOWER	41°			
THE MEAN VALUE IS	10.9					THE MEAN VALUE IS	45.			
LATITUDE 44 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	13					LATITUDE 44 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	43.			
LOWER	21°					LOWER	49°			
THE MEAN VALUE IS	17.					THE MEAN VALUE IS	49.			
LATITUDE 45 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	0					LATITUDE 45 NUMBER OF BT DISCONTINUITY LAYER, UPPER:	4			
LOWER	0.					LOWER	55°			
THE MEAN VALUE IS	0.					THE MEAN VALUE IS	58.			

Table C-6 (Concluded)

	TOTAL BT FOR NO	64	IS	22	TOTAL BT FOR DC	64	IS	0
1ST. OF MONTH NO	64	IS	22					
AVERAGE THERMOCLINE DATA FOLLOW				11				
LATITUDE 41 NUMBER OF BT	1							
DISCONTINUITY LAYER, UPPER:	15.							
LOWER	38.							
THE MEAN VALUE IS	7.9							
LATITUDE 42 NUMBER OF BT	11							
DISCONTINUITY LAYER, UPPER:	20.							
LOWER	39.							
THE MEAN VALUE IS	7.1							
LATITUDE 43 NUMBER OF BT	4							
DISCONTINUITY LAYER, UPPER:	37.							
LOWER	55.							
THE MEAN VALUE IS	5.9							
LATITUDE 44 NUMBER OF BT	4							
DISCONTINUITY LAYER, UPPER:	51.							
LOWER	67.							
THE MEAN VALUE IS	5.9							
LATITUDE 45 NUMBER OF BT	1							
DISCONTINUITY LAYER, UPPER:	70.							
LOWER	78.							
THE MEAN VALUE IS	74.							

TOTAL BT FOR 19 64 IS 459  
TOTAL THERMAL BT IS 101

Table C-7

TOTAL_BT	FOR	JA	65	IS	0	TOTAL_BT	FOR	AP	65	IS	0
TOTAL_BT FOR MY		65	15	30		TOTAL_BT FOR JU		65	IS	50	
ISO. OF MONTH MY		65	15	22		ISO. OF MONTH JU		65	IS	15	
AVERAGE THERMOCLINE DATA FOLLOW						AVERAGE THERMOCLINE DATA FOLLOW					
LATITUDE 41 NUMBER OF BT	5					LATITUDE 41 NUMBER OF BT	2				
DISCONTINUITY LAYER, UPPER:	10.					DISCONTINUITY LAYER, UPPER:	20.				
LOWER	16.					LOWER	23.				
THE MEAN VALUE IS	13.					THE MEAN VALUE IS	22.				
LATITUDE 42 NUMBER OF BT	1					LATITUDE 42 NUMBER OF BT	18				
DISCONTINUITY LAYER, UPPER:	18.					DISCONTINUITY LAYER, UPPER:	14.				
LOWER	23.					LOWER	21.				
THE MEAN VALUE IS	20.					THE MEAN VALUE IS	17.				
LATITUDE 43 NUMBER OF BT	1					LATITUDE 43 NUMBER OF BT	11				
DISCONTINUITY LAYER, UPPER:	12.					DISCONTINUITY LAYER, UPPER:	16.				
LOWER	16.					LOWER	24.				
THE MEAN VALUE IS	14.					THE MEAN VALUE IS	20.				
LATITUDE 44 NUMBER OF BT	1					LATITUDE 44 NUMBER OF BT	4				
DISCONTINUITY LAYER, UPPER:	10.					DISCONTINUITY LAYER, UPPER:	16.				
LOWER	14.					LOWER	27.				
THE MEAN VALUE IS	12.					THE MEAN VALUE IS	21.				
LATITUDE 45 NUMBER OF BT	0					LATITUDE 45 NUMBER OF BT	0				
DISCONTINUITY LAYER, UPPER:	0.					DISCONTINUITY LAYER, UPPER:	0.				
LOWER	0.					LOWER	0.				
THE MEAN VALUE IS	0.					THE MEAN VALUE IS	0.				
TOTAL_BT FOR JU	65	IS	37			TOTAL_BT FOR AU	65	IS	36		
ISO. OF MONTH JU	65	IS	4			ISO. OF MONTH AU	65	IS	5		
AVERAGE THERMOCLINE DATA FOLLOW						AVERAGE THERMOCLINE DATA FOLLOW					
LATITUDE 41 NUMBER OF BT	1					LATITUDE 41 NUMBER OF BT	0				
DISCONTINUITY LAYER, UPPER:	12.					DISCONTINUITY LAYER, UPPER:	0.				
LOWER	15.					LOWER	0.				
THE MEAN VALUE IS	13.					THE MEAN VALUE IS	0.				
LATITUDE 42 NUMBER OF BT	13					LATITUDE 42 NUMBER OF BT	11				
DISCONTINUITY LAYER, UPPER:	16.					DISCONTINUITY LAYER, UPPER:	0.				
LOWER	22.					LOWER	0.				
THE MEAN VALUE IS	19.					THE MEAN VALUE IS	21.				
LATITUDE 43 NUMBER OF BT	6					LATITUDE 43 NUMBER OF BT	5				
DISCONTINUITY LAYER, UPPER:	9.					DISCONTINUITY LAYER, UPPER:	22.				
LOWER	18.					LOWER	30.				
THE MEAN VALUE IS	13.					THE MEAN VALUE IS	26.				
LATITUDE 44 NUMBER OF BT	0					LATITUDE 44 NUMBER OF BT	15				
DISCONTINUITY LAYER, UPPER:	0.					DISCONTINUITY LAYER, UPPER:	16.				
LOWER	0.					LOWER	23.				
THE MEAN VALUE IS	0.					THE MEAN VALUE IS	20.				

Table C-7 (Concluded)

TOTAL BT FOR SP 65 IS 25	ISD. OF MONTH SP 65 IS 4	TOTAL BT FOR OC 65 IS 39
ISD. OF MONTH THERMOCLINE DATA FOLLOW	AVERAGE THERMOCLINE DATA FOLLOW	
LATITUDE 41 NUMBER OF BT 0	DISCONTINUITY LAYER, UPPER: 0.	DISCONTINUITY LAYER, LOWER: 0.
DISCONTINUITY LAYER, LOWER: 0.	THE MEAN VALUE IS 0.	THE MEAN VALUE IS 0.
LATITUDE 42 NUMBER OF BT 4	DISCONTINUITY LAYER, UPPER: 20.	DISCONTINUITY LAYER, LOWER: 17.4.
DISCONTINUITY LAYER, LOWER: 29.	THE MEAN VALUE IS 25.	THE MEAN VALUE IS 25.
LATITUDE 43 NUMBER OF BT 11	DISCONTINUITY LAYER, UPPER: 21.	DISCONTINUITY LAYER, LOWER: 13.7.
DISCONTINUITY LAYER, LOWER: 27.	THE MEAN VALUE IS 24.	THE MEAN VALUE IS 10.1.
LATITUDE 44 NUMBER OF BT 6	DISCONTINUITY LAYER, UPPER: 22.	DISCONTINUITY LAYER, LOWER: 13.7.
DISCONTINUITY LAYER, LOWER: 29.	THE MEAN VALUE IS 26.	THE MEAN VALUE IS 10.0.
LATITUDE 45 NUMBER OF BT 0	DISCONTINUITY LAYER, UPPER: 0.	DISCONTINUITY LAYER, LOWER: 0.
DISCONTINUITY LAYER, LOWER: 0.	THE MEAN VALUE IS 0.	THE MEAN VALUE IS 0.
TOTAL BT FOR NO 65 IS 63	ISD. OF MONTH NO 65 IS 18	TOTAL BT FOR OC 65 IS 0.
ISD. OF MONTH THERMOCLINE DATA FOLLOW	AVERAGE THERMOCLINE DATA FOLLOW	
LATITUDE 41 NUMBER OF BT 0	DISCONTINUITY LAYER, UPPER: 0.	DISCONTINUITY LAYER, LOWER: 0.
DISCONTINUITY LAYER, LOWER: 0.	THE MEAN VALUE IS 0.	THE MEAN VALUE IS 0.
LATITUDE 42 NUMBER OF BT 34	DISCONTINUITY LAYER, UPPER: 51.	DISCONTINUITY LAYER, LOWER: 58.
DISCONTINUITY LAYER, LOWER: 58.	THE MEAN VALUE IS 55.	THE MEAN VALUE IS 7.1.
LATITUDE 43 NUMBER OF BT 6	DISCONTINUITY LAYER, UPPER: 57.	DISCONTINUITY LAYER, LOWER: 58.
DISCONTINUITY LAYER, LOWER: 59.	THE MEAN VALUE IS 63.	THE MEAN VALUE IS 6.7.
LATITUDE 44 NUMBER OF BT 5	DISCONTINUITY LAYER, UPPER: 0.	DISCONTINUITY LAYER, LOWER: 0.
DISCONTINUITY LAYER, LOWER: 69.	THE MEAN VALUE IS 63.	THE MEAN VALUE IS 0.
TOTAL BT FOR 19 65 IS 280	TOTAL ISOTHERMAL BT IS 77	

Table C-8

TOTAL BT FOR ISO. OF MONTH MA	JA	66	IS	0
	MA	66	IS	26
	IS	26		
TOTAL BT FOR ISO. OF MONTH NY	NY	66	IS	23
	NY	66	IS	16
AVERAGE THERMOCLINE DATA FOLLOW				
LATITUDE 41 NUMBER OF BT	1			
DISCONTINUITY LAYER, UPPER:	4.			
LOWER	5.			
THE MEAN VALUE IS	5.			
LATITUDE 42 NUMBER OF BT	4			
DISCONTINUITY LAYER, UPPER:	12.			
LOWER	16.			
THE MEAN VALUE IS	14.			
LATITUDE 43 NUMBER OF BT	2			
DISCONTINUITY LAYER, UPPER:	3.			
LOWER	18.			
THE MEAN VALUE IS	10.			
LATITUDE 44 NUMBER OF BT	0			
DISCONTINUITY LAYER, UPPER:	0.			
LOWER	0.			
THE MEAN VALUE IS	0.			
LATITUDE 45 NUMBER OF BT	0			
DISCONTINUITY LAYER, UPPER:	0.			
LOWER	0.			
THE MEAN VALUE IS	0.			

TOTAL BT FOR ISO. OF MONTH AP	AP	66	IS	58
	AP	66	IS	53
AVERAGE THERMOCLINE DATA FOLLOW				
LATITUDE 41 NUMBER OF BT	1			
DISCONTINUITY LAYER, UPPER:	8.			
LOWER	9.			
THE MEAN VALUE IS	8.			
LATITUDE 42 NUMBER OF BT	3			
DISCONTINUITY LAYER, UPPER:	6.			
LOWER	37.			
THE MEAN VALUE IS	21.			
LATITUDE 43 NUMBER OF BT	1			
DISCONTINUITY LAYER, UPPER:	6.			
LOWER	9.			
THE MEAN VALUE IS	7.			
LATITUDE 44 NUMBER OF BT	0			
DISCONTINUITY LAYER, UPPER:	0.			
LOWER	0.			
THE MEAN VALUE IS	0.			
LATITUDE 45 NUMBER OF BT	0			
DISCONTINUITY LAYER, UPPER:	0.			
LOWER	0.			
THE MEAN VALUE IS	0.			

Table C-8 (Continued)

TOTAL_BT FOR SP 66 IS 18	TOTAL_BT FOR AU 66 IS 15	TOTAL_BT FOR OC 66 IS 173
TSG. OF MONTH SP 66 IS 6	TSG. OF MONTH AU 66 IS 6	TSG. OF MONTH OC 66 IS 50
AVERAGE THERMOCLINE DATA FOLLOW	AVERAGE THERMOCLINE DATA FOLLOW	AVERAGE THERMOCLINE DATA FOLLOW
LATITUDE 41 NUMBER OF BT 0	LATITUDE 41 NUMBER OF BT 0	LATITUDE 41 NUMBER OF BT 1
DISCONTINUITY LAYER, UPPER: 0.	DISCONTINUITY LAYER, UPPER: 0.	DISCONTINUITY LAYER, UPPER: 27.
LOWER: 0.	LOWER: 0.	LOWER: 30.
THE MEAN VALUE IS 0.	THE MEAN VALUE IS 0.	THE MEAN VALUE IS 28.
LATITUDE 42 NUMBER OF BT 7	LATITUDE 42 NUMBER OF BT 7	LATITUDE 42 NUMBER OF BT 56
DISCONTINUITY LAYER, UPPER: 27.	DISCONTINUITY LAYER, UPPER: 27.	DISCONTINUITY LAYER, UPPER: 32.
LOWER: 35.	LOWER: 35.	LOWER: 41.
THE MEAN VALUE IS 31.9	THE MEAN VALUE IS 31.9	THE MEAN VALUE IS 37.
LATITUDE 43 NUMBER OF BT 2	LATITUDE 43 NUMBER OF BT 2	LATITUDE 43 NUMBER OF BT 56
DISCONTINUITY LAYER, UPPER: 16.5	DISCONTINUITY LAYER, UPPER: 16.5	DISCONTINUITY LAYER, UPPER: 32.
LOWER: 25.	LOWER: 25.	LOWER: 43.
THE MEAN VALUE IS 23.	THE MEAN VALUE IS 23.	THE MEAN VALUE IS 38.
LATITUDE 44 NUMBER OF BT 3	LATITUDE 44 NUMBER OF BT 3	LATITUDE 44 NUMBER OF BT 8
DISCONTINUITY LAYER, UPPER: 16.9	DISCONTINUITY LAYER, UPPER: 16.9	DISCONTINUITY LAYER, UPPER: 22.
LOWER: 25.	LOWER: 25.	LOWER: 30.
THE MEAN VALUE IS 22.	THE MEAN VALUE IS 22.	THE MEAN VALUE IS 26.
LATITUDE 45 NUMBER OF BT 0	LATITUDE 45 NUMBER OF BT 0	LATITUDE 45 NUMBER OF BT 0
DISCONTINUITY LAYER, UPPER: 0.	DISCONTINUITY LAYER, UPPER: 0.	DISCONTINUITY LAYER, UPPER: 0.
LOWER: 0.	LOWER: 0.	LOWER: 0.
THE MEAN VALUE IS 0.	THE MEAN VALUE IS 0.	THE MEAN VALUE IS 0.

Table C-8 (Concluded)

TOTAL BT FOR 150° OF MONTH NO	66 IS	27 IS	TOTAL BT FOR 150° OF MONTH NO	66 DC	66 IS	TOTAL BT FOR 150° OF MONTH NO	66 DC	66 IS	TOTAL BT FOR 150° OF MONTH NO	66 DC	66 IS
AVERAGE THERMOCLINE DATA FOLLOW											
LATITUDE 41 NUMBER OF BT DISCONTINUITY LAYER, UPPER: 1											
DISCONTINUITY LAYER, LOWER: 22.											
THE MEAN VALUE IS 24.											
LATITUDE 42 NUMBER OF BT DISCONTINUITY LAYER, UPPER: 10											
DISCONTINUITY LAYER, LOWER: 46.											
THE MEAN VALUE IS 46.											
LATITUDE 43 NUMBER OF BT DISCONTINUITY LAYER, UPPER: 1											
DISCONTINUITY LAYER, LOWER: 75.											
THE MEAN VALUE IS 85.											
LATITUDE 44 NUMBER OF BT DISCONTINUITY LAYER, UPPER: 4											
DISCONTINUITY LAYER, LOWER: 75.											
THE MEAN VALUE IS 60.											
LATITUDE 45 NUMBER OF BT DISCONTINUITY LAYER, UPPER: 0											
DISCONTINUITY LAYER, LOWER: 0.											
THE MEAN VALUE IS 0.											
<u>TOTAL BT FOR 19 IS 444</u>											
<u>TOTAL ISOTHERMAL BT IS 189</u>											

Table C-9

TOTAL_BT FOR 1ST. OF MONTH	JAN	67	IS	57
TOTAL_BT FOR 1ST. OF MONTTH	JAN	67	IS	6
TOTAL_BT FOR 1ST. OF MONTTH	MAR	67	IS	6
TOTAL_BT FOR 1ST. OF MONTTH	MAY	67	IS	6
TOTAL_BT FOR 1ST. OF MONTTH	JULY	67	IS	6
TOTAL_BT FOR 1ST. OF MONTTH	SEP.	67	IS	38
			AVERAGE THERMOCINE DATA FOLLOW	
LATITUDE 41 NUMBER OF BT DISCONTINUITY LAYER, UPPER:		9		8.
LATITUDE 41 NUMBER OF BT DISCONTINUITY LAYER, LOWER:		9		13.
			THE MEAN VALUE IS	11.
LATITUDE 42 NUMBER OF BT DISCONTINUITY LAYER, UPPER:		5		22.
LATITUDE 42 NUMBER OF BT DISCONTINUITY LAYER, LOWER:		5		28.
			THE MEAN VALUE IS	25.
LATITUDE 43 NUMBER OF BT DISCONTINUITY LAYER, UPPER:		3		5.
LATITUDE 43 NUMBER OF BT DISCONTINUITY LAYER, LOWER:		3		10.
			THE MEAN VALUE IS	8.
LATITUDE 44 NUMBER OF BT DISCONTINUITY LAYER, UPPER:		2		13.
LATITUDE 44 NUMBER OF BT DISCONTINUITY LAYER, LOWER:		2		34.
			THE MEAN VALUE IS	23.
LATITUDE 45 NUMBER OF BT DISCONTINUITY LAYER, UPPER:		0		0.
LATITUDE 45 NUMBER OF BT DISCONTINUITY LAYER, LOWER:		0		0.
			THE MEAN VALUE IS	

TOTAL BT FOR FF	67	IS.	0
ISO. OF MONTH	AP	67	IS.
AVERAGE THERMOCLINE DATA FOLLOW	AP	67	IS.
LATITUDE 42 NUMBER OF BT	15	IS.	36
DISCONTINUITY LAYER, UPPER:	5.	IS.	6.0
LOWER	7.	IS.	5.6
THE MEAN VALUE IS	6.	IS.	5.8
LATITUDE 43 NUMBER OF BT	1	IS.	7.9
DISCONTINUITY LAYER, UPPER:	6.	IS.	7.3
LOWER	9.	IS.	7.6
THE MEAN VALUE IS	7.	IS.	7.6
LATITUDE 44 NUMBER OF BT	0	IS.	0.0
DISCONTINUITY LAYER, UPPER:	0.	IS.	0.0
LOWER	0.	IS.	0.0
THE MEAN VALUE IS	0.	IS.	0.0
LATITUDE 45 NUMBER OF BT	0	IS.	0.0
DISCONTINUITY LAYER, UPPER:	0.	IS.	0.0
LOWER	0.	IS.	0.0
THE MEAN VALUE IS	0.	IS.	0.0
BT 1671 IS AN ISOTHERMAL BT			
TOTAL AT ECR JU	67	IS.	6.3
ISO. OF MONTH JU	67	IS.	14
AVERAGE THERMOCLINE DATA FOLLOW			
LATITUDE 41 NUMBER OF BT FOLLOW	2	IS.	
DISCONTINUITY LAYER, UPPER:	6.	IS.	14.0
LOWER	10.	IS.	8.8
THE MEAN VALUE IS	8.	IS.	11.4
LATITUDE 43 NUMBER OF BT	15	IS.	14.5
DISCONTINUITY LAYER, UPPER:	10.	IS.	11.0
LOWER	15.	IS.	6.6
THE MEAN VALUE IS	11.	IS.	12.8
LATITUDE 44 NUMBER OF BT	3	IS.	
DISCONTINUITY LAYER, UPPER:	12.	IS.	
LOWER	21.	IS.	7.8
THE MEAN VALUE IS	16.	IS.	6.9

Table C-9 (Continued)

TOTAL_BT_ECR_JL	67	IS	57				
ISO. OF MONTH_JL	67	IS	8				
AVERAGE THERMOCLINE DATA FOLLOW							
LATITUDE 41 NUMBER OF BT	5						
DISCONTINUITY LAYER, UPPER:	10.		21.2				
LOWER	12.		15.2				
THE MEAN VALUE IS	11.		18.2				
LATITUDE 42 NUMBER OF BT	22						
DISCONTINUITY LAYER, UPPER:	12.		17.7				
LOWER	15.		10.2				
THE MEAN VALUE IS	13.		13.9				
LATITUDE 43 NUMBER OF BT	7						
DISCONTINUITY LAYER, UPPER:	11.		17.8				
LOWER	15.		10.5				
THE MEAN VALUE IS	13.		14.1				
LATITUDE 44 NUMBER OF BT	6						
DISCONTINUITY LAYER, UPPER:	12.		14.8				
LOWER	16.		8.4				
THE MEAN VALUE IS	14.		11.6				
LATITUDE 45 NUMBER OF BT	9						
DISCONTINUITY LAYER, UPPER:	10.		14.3				
LOWER	16.		9.1				
THE MEAN VALUE IS	13.		11.7				
TOTAL_BT_ECR_SP	67	IS	25				
ISO. OF MONTH_SP	67	IS	1				
AVERAGE THERMOCLINE DATA FOLLOW							
LATITUDE 41 NUMBER OF BT	2						
DISCONTINUITY LAYER, UPPER:	18.		17.5				
LOWER	22.		14.0				
THE MEAN VALUE IS	20.		15.7				
LATITUDE 42 NUMBER OF BT	11						
DISCONTINUITY LAYER, UPPER:	21.		16.5				
LOWER	26.		9.2				
THE MEAN VALUE IS	23.		12.9				
LATITUDE 43 NUMBER OF BT	0						
DISCONTINUITY LAYER, UPPER:	0.		0.0				
LOWER	0.		0.0				
THE MEAN VALUE IS	0.		0.0				
LATITUDE 44 NUMBER OF BT	9						
DISCONTINUITY LAYER, UPPER:	17.		13.4				
LOWER	27.		6.4				
THE MEAN VALUE IS	22.		9.9				
LATITUDE 45 NUMBER OF BT	2						
DISCONTINUITY LAYER, UPPER:	21.		15.4				
LOWER	30.		6.0				
THE MEAN VALUE IS	26.		10.7				

TOTAL_BT_ECR_AU	67	IS	63				
ISO. OF MONTH_AU	67	IS	8				
AVERAGE THERMOCLINE DATA FOLLOW							
LATITUDE 41 NUMBER OF BT	9						
DISCONTINUITY LAYER, UPPER:			13.				
LCMFR	14.		19.7				
THE MEAN VALUE IS	13.		16.5				
LATITUDE 42 NUMBER OF BT	8						
DISCONTINUITY LAYER, UPPER:			18.				
LOWER	20.		11.1				
THE MEAN VALUE IS	19.		16.9				
LATITUDE 43 NUMBER OF BT	36						
DISCONTINUITY LAYER, UPPER:			14.				
LCMFR	19.		16.9				
THE MEAN VALUE IS	17.		17.6				
LATITUDE 44 NUMBER OF BT	2						
DISCONTINUITY LAYER, UPPER:			15.				
LCMFR	18.		17.0				
THE MEAN VALUE IS	17.		14.2				
LATITUDE 45 NUMBER OF BT	0						
DISCONTINUITY LAYER, UPPER:			0.				
LCMFR	0.		0.0				
THE MEAN VALUE IS	0.		0.0				
TOTAL_BT_ECR_OC	67	IS	102				
ISO. OF MONTH_OC	67	IS	45				
AVERAGE THERMOCLINE DATA FOLLOW							
LATITUDE 41 NUMBER OF BT	0						
DISCONTINUITY LAYER, UPPER:			0.				
LOWER	42.		6.0				
THE MEAN VALUE IS	40.		8.7				
LATITUDE 42 NUMBER OF BT	19						
DISCONTINUITY LAYER, UPPER:			38.				
LOWER	42.		11.4				
THE MEAN VALUE IS	49.		5.1				
LATITUDE 43 NUMBER OF BT	7						
DISCONTINUITY LAYER, UPPER:			23.				
LOWER	33.		11.0				
THE MEAN VALUE IS	28.		8.5				
LATITUDE 44 NUMBER OF BT	4						
DISCONTINUITY LAYER, UPPER:			20.				
LOWER	34.		11.3				
THE MEAN VALUE IS	27.		9.7				

Table C-9 (Concluded)

TOTAL BT FOR NO.	67	IS	5		TOTAL BT FOR DC.	67	IS	0
ISO. OF MONTH NO.	67	IS	2					
AVERAGE THERMOCLINE DATA FOLLOW								
LATITUDE 41 NUMBER OF BT	0							
DISCONTINUITY LAYER, UPPER:	0.		0.0					
LOWER	0.		0.0					
THE MEAN VALUE IS	0.		0.0					
LATITUDE 42 NUMBER OF BT	2							
DISCONTINUITY LAYER, UPPER:	30.		9.7					
LOWER	39.		5.4					
THE MEAN VALUE IS	35.		7.6					
LATITUDE 43 NUMBER OF BT	0							
DISCONTINUITY LAYER, UPPER:	0.		0.0					
LOWER	0.		0.0					
THE MEAN VALUE IS	0.		0.0					
LATITUDE 44 NUMBER OF BT	0							
DISCONTINUITY LAYER, UPPER:	0.		0.0					
LOWER	0.		0.0					
THE MEAN VALUE IS	0.		0.0					
LATITUDE 45 NUMBER OF BT	1		10.7					
DISCONTINUITY LAYER, UPPER:	45.							
LOWER	50.		6.7					
THE MEAN VALUE IS	47.		8.7					

TOTAL BT AT EQ. IS 67 IS 41.7  
TOTAL ISOTHERMAL BT IS 15.9



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